



WHY IS STABILITY IMPORTANT IN SOLIDS?

IN DESIGN WE GENERALLY ADDRESS TWO ISSUES:

- **CHECK OPERATING LOADS** (STRESSES WITHIN ELASTIC LIMITS)
- **DESIGN TO AVOID FAILURE** (SAFETY AT EXTREME LOADS)

FAILURE OF STRUCTURES FALLS INTO TWO BASIC TYPES:

- **FRACTURE** (STRESS CONCENTRATION AT **LOCAL FLAWS**)
- **BUCKLING** (**OVERALL** STRUCTURAL FAILURE DUE TO **INSTABILITY**)

REASON FOR BUCKLING INSTABILITY: NONLINEAR BEHAVIOR OF STRUCTURES

STUDY OF STABILITY IMPORTANT NOT ONLY FOR ENGINEERING STRUCTURES, BUT FOR A MUCH WIDER RANGE OF APPLICATIONS IN SOLIDS AND MATERIALS



COURSE OVERVIEW

1. **Concept of stability and examples of discrete systems**
2. **Concept of bifurcation and examples of discrete, conservative systems**
3. **LSK asymptotics for perfect continua & 1D application (elastica) – simple mode case**
4. **2D application (plate) & LSK asymptotics for imperfect continua – simple mode case**
5. **LSK asymptotics for perfect continua & 2D application (plate) – multiple mode case**
6. **FEM techniques for continuum elastic systems. Buckling of fiber-reinforced composites**
7. **Stability of honeycomb under compressive loading – Bloch wave representation**
8. **Phase transformations in shape memory alloys: continuum & 3D lattice models**
9. **Review**



NEW CONCEPTS INTRODUCED

1. Concept of **stability** (here of an **equilibrium**)
 1. **Linearization** method
 2. **Lyapunov's direct** method
2. Concept of **bifurcation** (here for equilibria of **conservative**, elastic systems)
 1. **Limit point vs bifurcation point**
 2. **Imperfections** change **bifurcation** to **limit** points (or **lower singularity** order)
 3. Imperfections: **amplitude vs shape**
3. **LSK asymptotics** for continuum conservative systems : **reduce** study of an **infinite** problem to the study of a **finite-dimensional** one near the critical point.



STABILITY OF EQUILIBRIUM STATES



TWO WIDELY USED METHODS TO CHECK STABILITY:

1. LINEARIZATION METHOD

- a) **Linearization** of the equations of motion about equilibrium state
- b) Stability analysis of the linearized perturbed motions

STABILITY if all eigenvalues have non-positive real part

- c) **Justification** of the results with respect to the actual motion of the system
-

2. LYAPUNOV'S DIRECT METHOD

STABILITY guaranteed when a non-increasing functional $L(p(t))$ can be found that satisfies certain bounding properties for the initial conditions and the current state



LINEARIZATION METHOD

$$\dot{\mathbf{p}} = \mathbf{f}(\mathbf{p}) = \mathbf{f}(\mathbf{p}_e) + \left[\frac{\partial \mathbf{f}}{\partial \mathbf{p}} \right]_e [\mathbf{p} - \mathbf{p}_e] + \mathbf{o}(\|\mathbf{p} - \mathbf{p}_e\|), \quad \text{Taylor series expansion of } \mathbf{f}$$

$$0 = \mathbf{f}(\mathbf{p}_e), \quad \text{recall from equilibrium}$$

$$\Delta \mathbf{p} \equiv \mathbf{p} - \mathbf{p}_e, \quad \mathbf{A} \equiv \left[\frac{\partial \mathbf{f}}{\partial \mathbf{p}} \right]_e, \quad \text{definitions}$$

$$\Delta \dot{\mathbf{p}} = \mathbf{A} \Delta \mathbf{p}, \quad \text{LINEARIZED SYSTEM (approximates actual one)}$$

$$\Delta \mathbf{p}(t) = \exp[t\mathbf{A}] \Delta \mathbf{p}(0), \quad \text{solution of linearized system}$$

$$\Delta \mathbf{p}(t) \text{ bounded } \forall t > 0 \text{ iff } \Re(a_i) < 0 \forall \text{ eigenvalues } a_i \text{ of } \mathbf{A}$$

**STABILITY OF
LINEARIZED SYSTEM**

NOTE : for simplicity $\partial \mathbf{f} / \partial t = 0$, autonomous system $\implies \mathbf{A}$ is a constant matrix



LINEARIZATION METHOD (LYAPUNOV'S THEOREM)

- If the real part of **all** the eigenvalues a_i of the linearized system's matrix A are **negative**, (not necessarily strictly so) the system is **stable**
- If the real part of at least **one** eigenvalue a_i of the linearized system's matrix A is **strictly positive**, the system is **unstable**

NOTE: Proof of stability for nonlinear system requires additional information about the growth of the difference between the linearized and nonlinear systems



LYAPUNOV'S DIRECT METHOD

A system is **stable** if a functional $L(\mathbf{p}(t))$ **can be found** with the following properties:

- $\frac{dL}{dt} \leq 0$, (functional is nonincreasing)
- $L(\mathbf{p}(t)) \geq c \|\mathbf{p}(t) - \mathbf{p}_e\|^2$, ($c > 0$; functional measures distance from equilibrium)
- $L(\mathbf{p}(0)) \leq d \|\mathbf{p}(0) - \mathbf{p}_e\|^2$, ($d > 0$; functional measures initial perturbation)

PROOF :

$$c \|\mathbf{p}(t) - \mathbf{p}_e\|^2 \leq L(\mathbf{p}(t)) \leq L(\mathbf{p}(0)) \leq d \|\mathbf{p}(0) - \mathbf{p}_e\|^2 \implies \|\mathbf{p}(t) - \mathbf{p}_e\| \leq \varepsilon; (\eta \leq \varepsilon \sqrt{c/d})$$

NOTE: Finding a Lyapunov functional for a stable system is **not always** possible

CONSERVATIVE SYSTEM IS **STABLE IFF POTENTIAL ENERGY **MINIMIZED** AT EQUILIBRIUM**

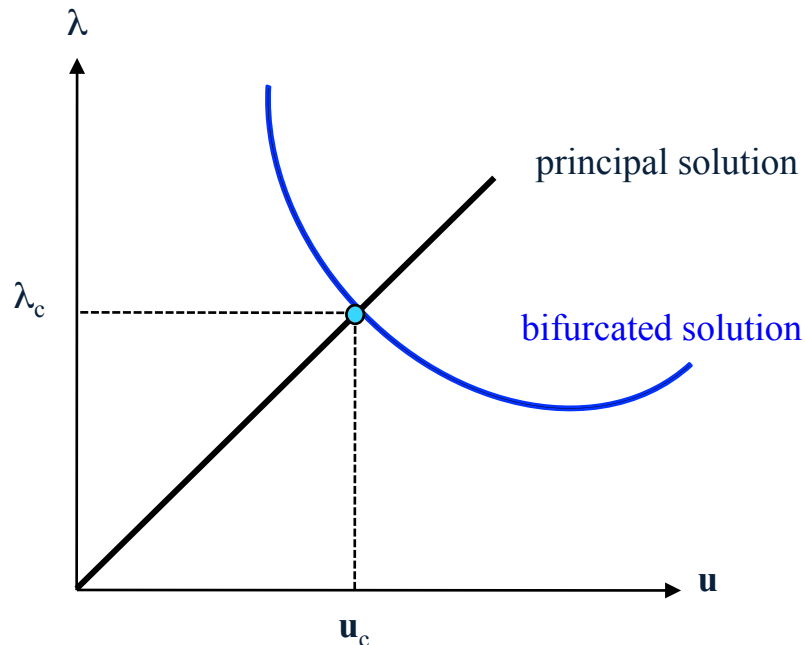


BIFURCATION OF EQUILIBRIUM SOLUTIONS IN CONSERVATIVE, NONLINEAR SYSTEMS



FUNDAMENTAL ASSUMPTIONS USED:

- Systems are **time-independent**
- Systems are **conservative**, i.e. they have an **energy** which remains constant
- Energy depends on a scalar parameter λ (termed **load parameter**)
- Systems are **nonlinear**, i.e. energy is **non-quadratic** function of independent variable and as a result for a given λ , **multiple equilibrium solutions** can be found
- **Stability** of these equilibrium solutions are examined by investigating if their **energy** has a **local minimum** at these solutions



BIFURCATION: Loss of uniqueness – as a function of a control parameter – in the solution of a nonlinear system of equations. Bifurcated branch typically emerges as a “fork” from the principal branch.

- System: $\mathbf{f}(\mathbf{u}, \lambda) = \mathbf{0}$
- Principal solution starts at $\lambda = 0, \mathbf{u} = \mathbf{0}$
- Bifurcated solution emerges from principal one at the **critical point** λ_c

$\mathcal{E}(\mathbf{u}, \lambda)$: energy of system at displacement $\mathbf{u} \in \mathbb{R}^n$ and load $\lambda \geq 0$

$\mathbf{f}(\mathbf{u}, \lambda) \equiv \mathcal{E}_{,\mathbf{u}} = \mathbf{0}$, equilibrium is energy extremum : $\mathcal{E}_{,\mathbf{u}} \equiv \partial \mathcal{E} / \partial \mathbf{u}$

$\mathbf{u}^0(\lambda)$: principal solution i.e. $\mathbf{f}(\mathbf{u}^0(\lambda), \lambda) = \mathbf{0}, \forall \lambda \geq 0; \mathbf{u}^0(0) = \mathbf{0}$

$\mathcal{E}_{,\mathbf{u}\mathbf{u}} \Delta \mathbf{u} + \mathcal{E}_{,\mathbf{u}\lambda} \Delta \lambda \approx \mathbf{0} \implies \Delta \mathbf{u} \approx -\Delta \lambda [\mathcal{E}_{,\mathbf{u}\mathbf{u}}]^{-1} [\mathcal{E}_{,\mathbf{u}\lambda}]$; construct $\mathbf{u}^0(\lambda)$ by continuation



MEC 563 - STABILITY OF SOLIDS - REVIEW

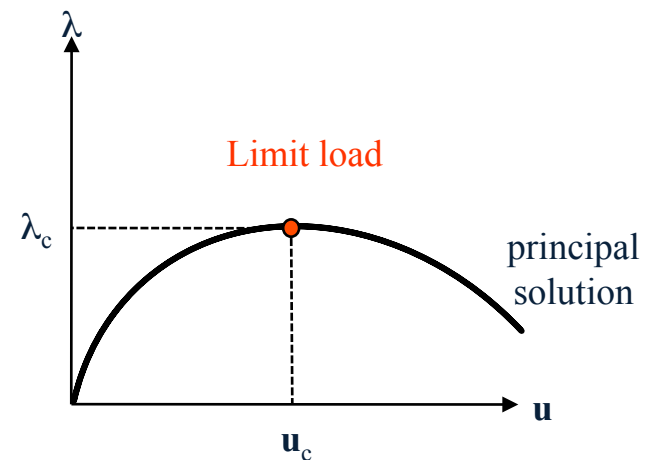
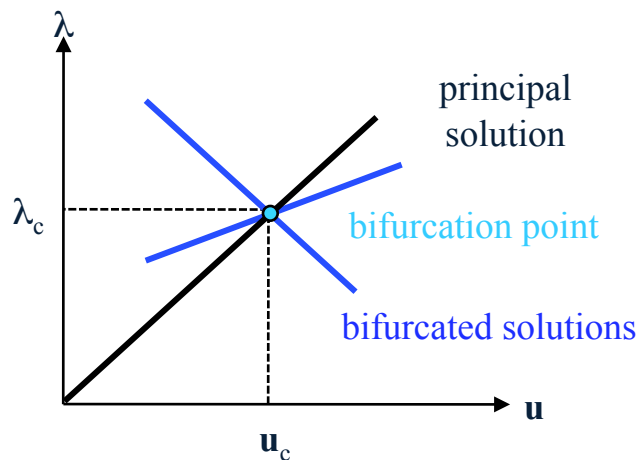


$$\mathcal{E}^c_{,\mathbf{u}\mathbf{u}} \equiv \left[\frac{\partial^2 \mathcal{E}(\mathbf{u}, \lambda)}{\partial \mathbf{u} \partial \mathbf{u}} \right]_{(\mathbf{u}^0(\lambda_c), \lambda_c)} \text{ non - invertible at } \mathbf{u}^0(\lambda_c) \implies \text{principal solution singularity}$$

$$[\mathcal{E}^c_{,\mathbf{u}\mathbf{u}}][\mathbf{u}^{(i)}] = \mathbf{0}, \quad i = 1, \dots, m; \quad \lambda_c : \text{critical load}, \quad \mathbf{u}^{(i)} : \text{critical mode}, \quad m : \text{multiplicity}$$

if : $[\mathcal{E}^c_{,\mathbf{u}\lambda}][\mathbf{u}^{(i)}] = 0 \implies$ bifurcation at λ_c

if : $[\mathcal{E}^c_{,\mathbf{u}\lambda}][\mathbf{u}^{(i)}] \neq 0 \implies$ limit load at λ_c



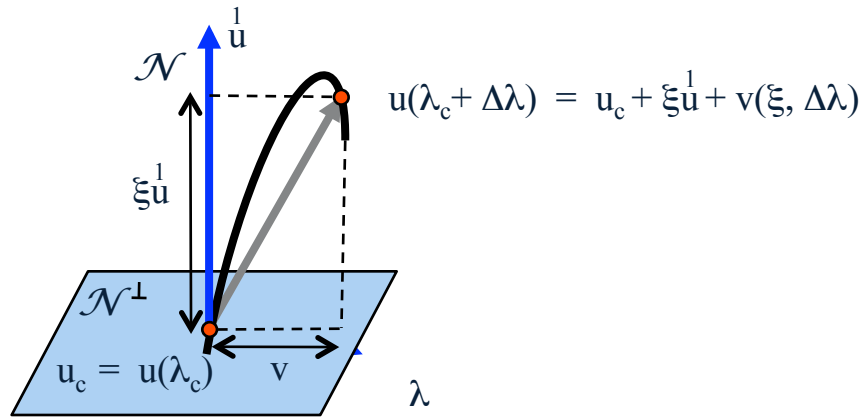


LSK (LYAPUNOV - SCHMIDT - KOITER) ASYMPTOTICS

- General asymptotic method to study motion of systems (discrete or continuous) near singular points. Here the method is applied to the **equilibrium** of **conservative elastic** systems.
- **IDEA**: Study the **projection** of equilibrium equations along the **finite dimensional null space** of the system's stability operator at critical point. This way the study of a large problem is **reduced to the study of a nonlinear system of m equations**, where m is the multiplicity of the stability operator's eigenvalue at the critical point.
- Method **follows asymptotically equilibrium paths** emerging from bifurcation points (simple or multiple) of **perfect** systems and determines their **stability**.
- Method also **investigates** the **equilibrium** and **stability** of **imperfect** systems, near critical points of their perfect counterparts, for **small imperfection amplitudes**.
- **NOTE**: Method is useful in determining **post-bifurcation behavior** and **imperfection sensitivity** in applications as well as in providing efficient **numerical tools** for finding solutions near the singular points of complex nonlinear systems.

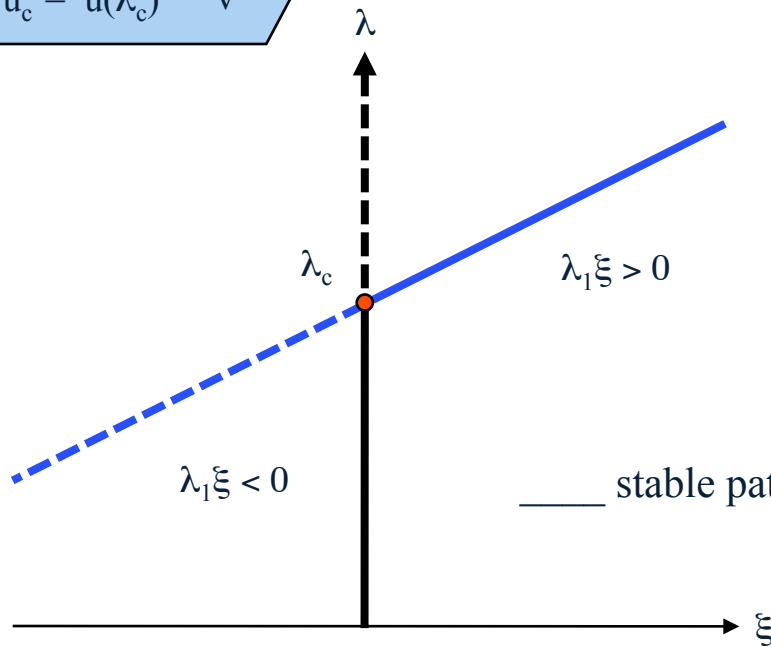


ASYMPTOTIC EXPANSIONS – SIMPLE BIFURCATION CASE

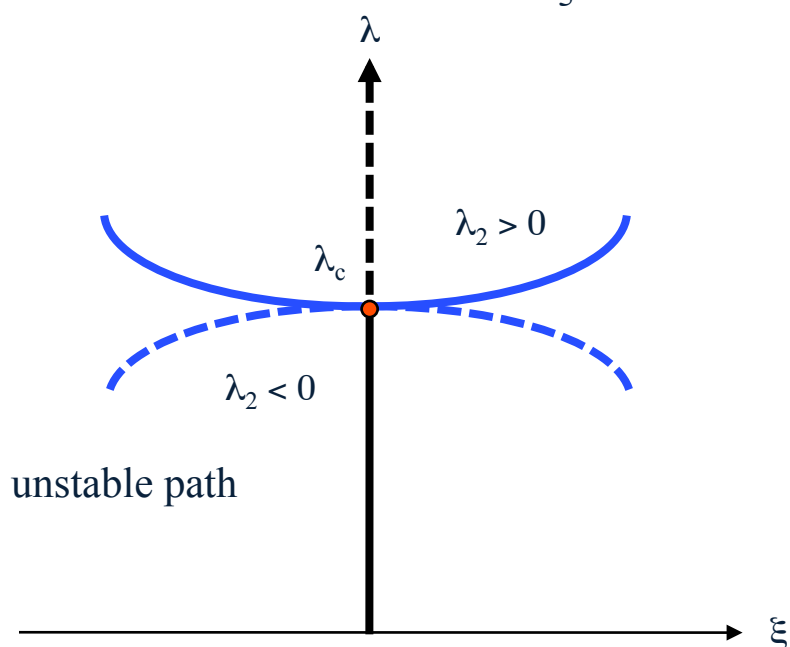


- About critical point u_c project solution increment Δu along null space \mathcal{N} and its complement \mathcal{N}^\perp .

- Solve equilibrium in \mathcal{N}^\perp and use $v(\xi, \Delta\lambda)$ to find equilibrium in \mathcal{N} from which you determine $\Delta\lambda$ as a function of ξ



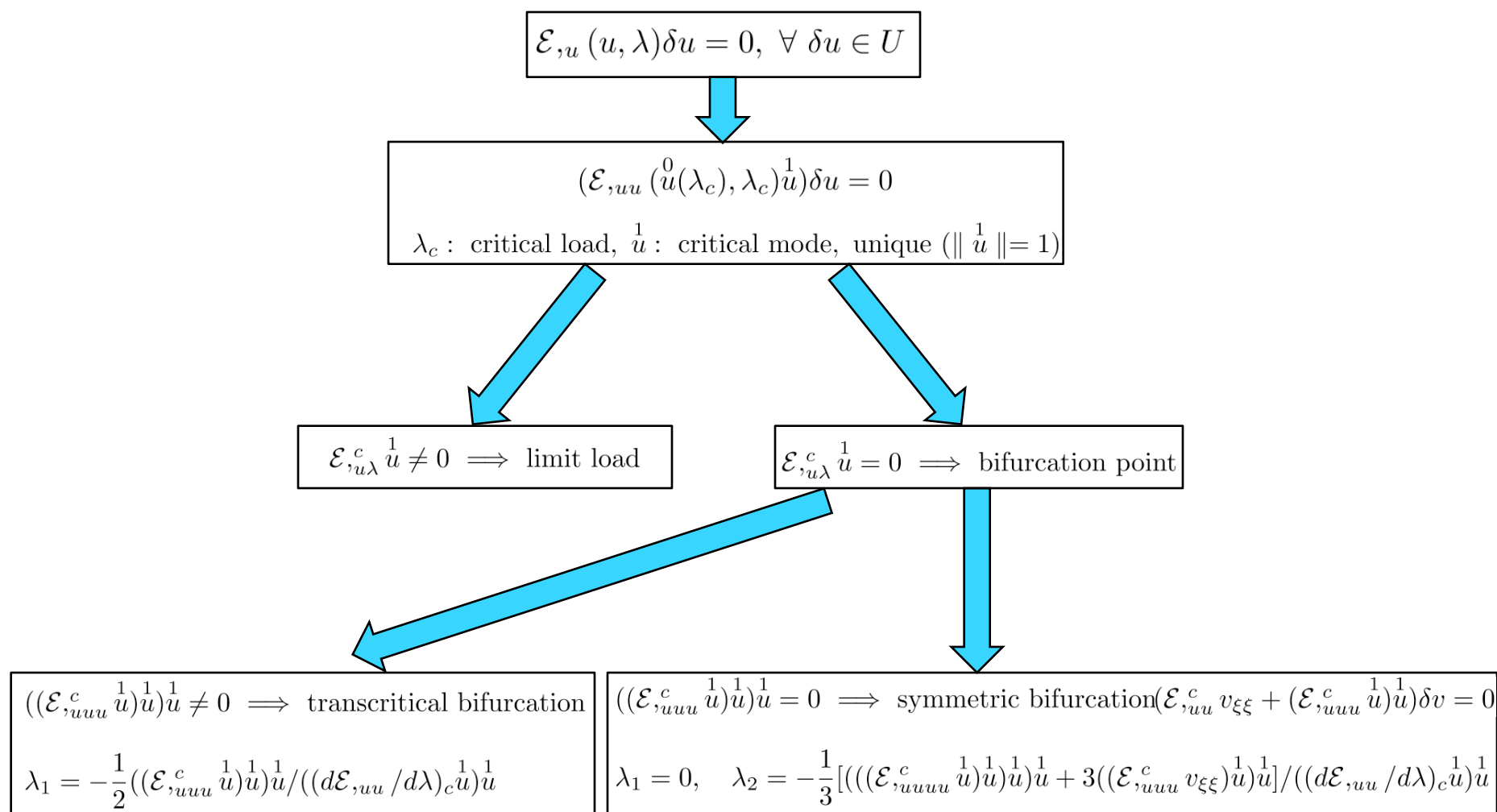
ASYMMETRIC BIFURCATION



SYMMETRIC BIFURCATION

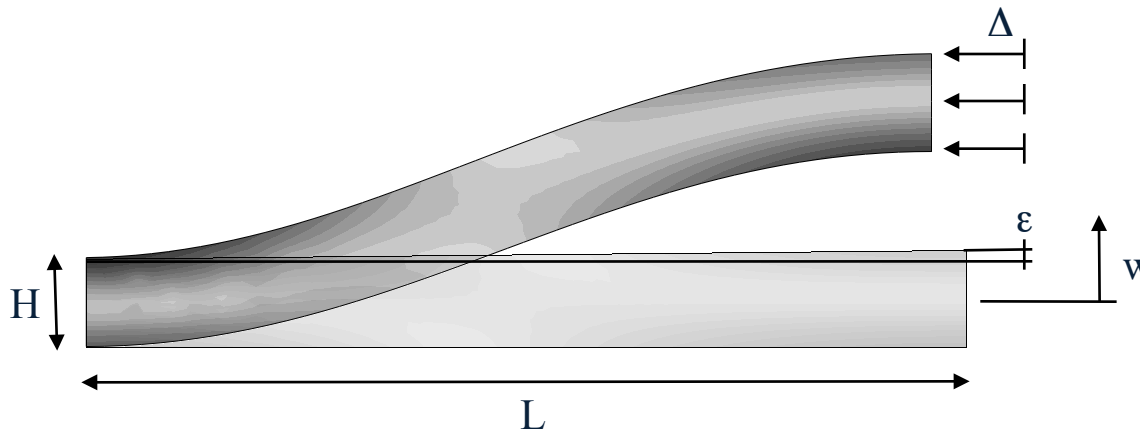


ASYMPTOTIC EXPANSIONS – SIMPLE BIFURCATION CASE





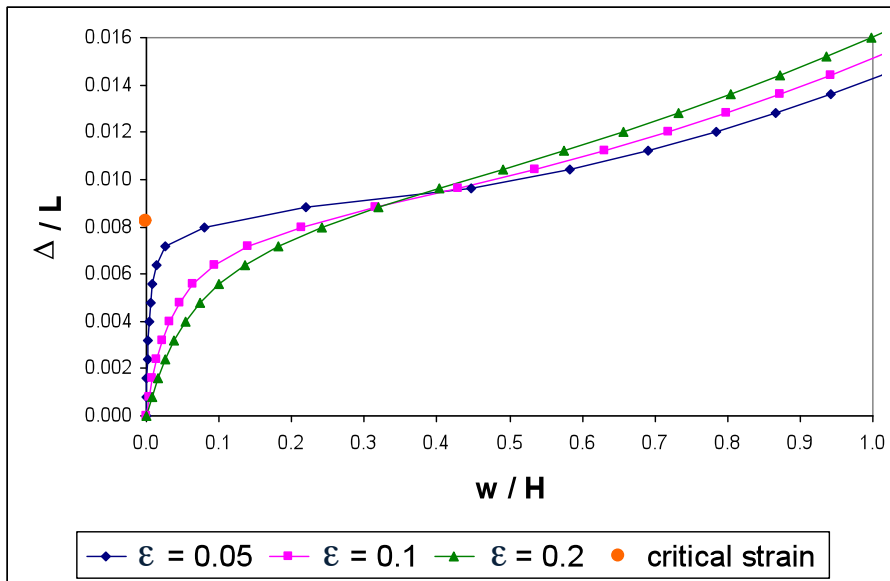
CONCEPT OF IMPERFECTION – ILLUSTRATION



Beam slenderness: $L/H = 10$

Imperfection $\varepsilon = \Delta H/H$

NOTE: Different types of imperfections can be used, geometric or material – all are equivalent



Deformation of an axially compressed beam that has a slight geometric imperfection (beam is trapezoidal with an imperfection angle $\varepsilon = \Delta H/H$)

As imperfection amplitude ε decreases, equilibrium approaches perfect case

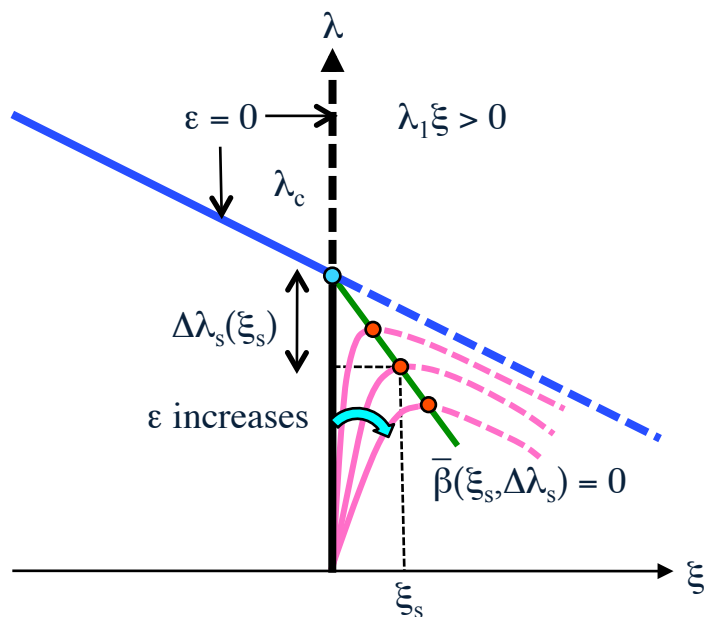


LSK ASYMPTOTICS – IMPERFECTIONS – SIMPLE MODE

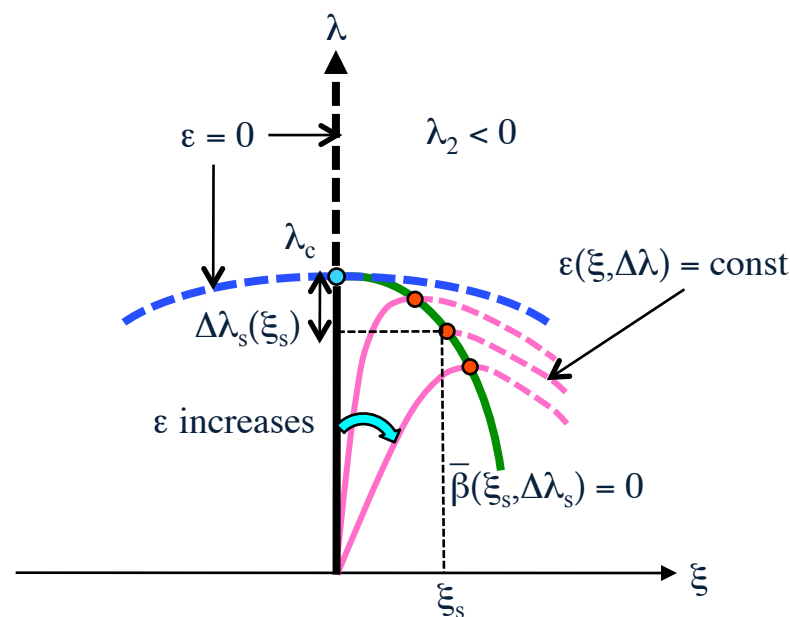
- Behavior of **imperfect** structure near critical load can be **analyzed** by **asymptotic expansion** of equilibrium solution.
- **Bifurcation** point in perfect case is **replaced** by **limit points** in imperfect case.
- Method determines the limit points (where stability changes) of imperfect structure and the **load drop** $\Delta\lambda_s$ from the critical load of the perfect structure λ_c to the maximum load of the imperfect one λ_s .
- Recall that in real structures the amplitude ε can be controlled but **not** the shape w .
- Load drop is **maximized** when **imperfection has the shape of the eigenmode**.
- Structures are **imperfection sensitive** (i.e. $\Delta\lambda_s < 0$) for **asymmetric** or **symmetric subcritical** bifurcations (load max exists for the equilibrium path through zero load); $\Delta\lambda_s = O(\varepsilon^{1/2})$ for asymmetric case and $\Delta\lambda_s = O(\varepsilon^{2/3})$ for subcritical symmetric case.
- **NOTE:** Imperfection can occur in **any property** (material or geometric) that **destroys** the **symmetry** of the system; all related asymptotic analyses are equivalent.



IMPERFECTIONS – SIMPLE MODE – GENERAL RESULTS



Asymmetric bifurcation – Imperfect Case



Symmetric bifurcation – Imperfect Case

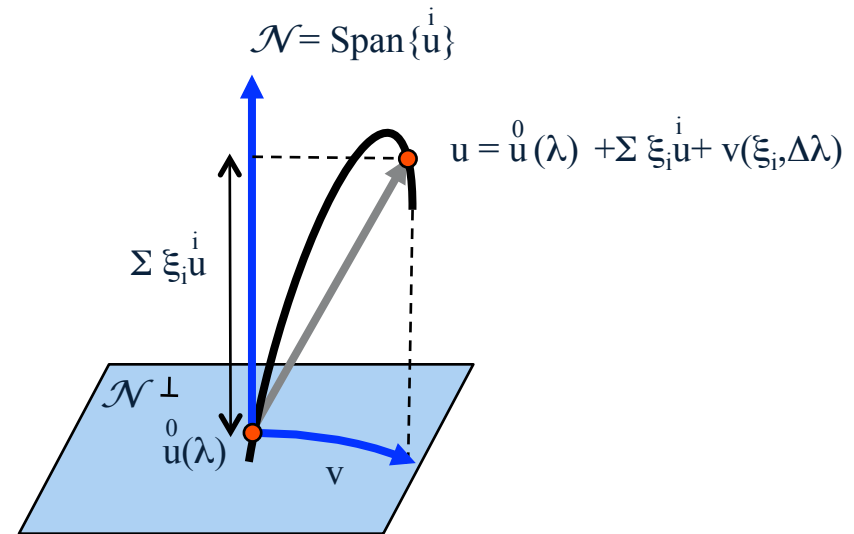
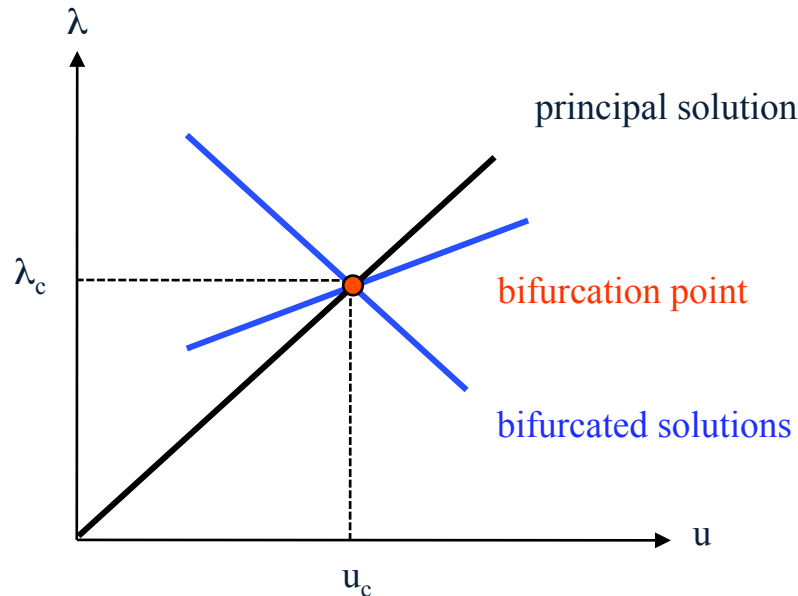


ASYMPTOTIC EXPANSIONS – MULTIPLE BIFURCATION CASE

- **Interest** of multiple mode case for applications: systems with an **initially high symmetry**: e.g. cylinder buckling, stability of cubic crystals.
- **IDEA**: Study the **projection** of equilibrium equations along the **finite dimensional null space** of the system's stability operator at critical point. This way the study of a large problem is **reduced to the study of a nonlinear system of m equations** where m is the multiplicity of the stability operator's eigenvalue at the critical point.
- Method **follows asymptotically all the equilibrium paths** emerging from the bifurcation point of the perfect system and **determines their stability**.
- Method also investigates the **equilibrium and stability of imperfect** systems, near critical points of their perfect counterparts, for **small imperfection amplitudes**
- **NOTE**: Method is useful in determining **post-bifurcation behavior** and **imperfection sensitivity** in applications as well as in providing efficient **numerical tools** for finding solutions near the singular points of complex nonlinear systems with a **high degree of initial symmetry**



ASYMPTOTIC EXPANSIONS – MULTIPLE BIFURCATION CASE



Method is a straightforward **generalization** of **simple mode** case:

- About an arbitrary point $\lambda = \lambda_c + \Delta\lambda$ of the principal solution $u^0(\lambda)$ project difference $\Delta u = u - u^0$ along m -dimensional null space \mathcal{N} and its orthogonal complement \mathcal{N}^\perp . Subsequently expand corresponding equilibrium equations about λ_c
- From critical point u_c, λ_c **at most** $2^m - 1$ (asymmetric case) or $(3^m - 1)/2$ (symmetric case) bifurcated equilibrium paths emerge (because initial tangents are solutions of m 2nd or 3rd order polynomial equations with m variables)

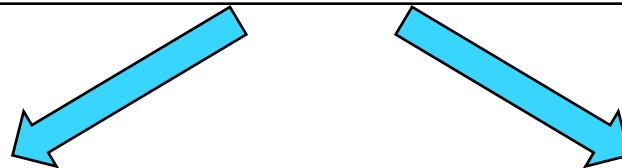


ASYMPTOTIC EXPANSIONS – MUTIPLE BIFURCATION CASE

$$\mathcal{E}_{,u}(u, \lambda)\delta u = 0, \quad \forall \delta u \in U$$

$$(\mathcal{E}_{,uu}(\overset{0}{u}(\lambda_c), \lambda_c)\overset{i}{u})\delta u = 0, \quad (\overset{i}{u}, \overset{j}{u}) = \delta_{ij}; \quad 1 \leq i, j \leq m$$

$$\mathcal{E}_{,u\lambda}^c \overset{i}{u} = 0, \quad 1 \leq i \leq m; \quad m - \text{tuple bifurcation point at : } (u_c, \lambda_c)$$



case (i) : $\mathcal{E}_{ijk} \neq 0, \exists(i, j, k)$

$$\sum_{j=1}^m \sum_{k=1}^m \alpha_j^1 \alpha_k^1 \mathcal{E}_{ijk} + 2\lambda_1 \sum_{j=1}^m \alpha_j^1 \mathcal{E}_{ij\lambda} = 0, \quad \sum_{i=1}^m (\alpha_i^1)^2 = 1$$

$$B_{ij} \equiv \sum_{k=1}^m \alpha_k^1 \mathcal{E}_{ijk} + \lambda_1 \mathcal{E}_{ij\lambda}$$

Branch unstable for different sign eigenvalues

case (ii) : $\mathcal{E}_{ijk} = 0, \forall(i, j, k)$

$$\lambda_1 = 0, \quad \sum_{j=1}^m \sum_{k=1}^m \sum_{l=1}^m \alpha_j^1 \alpha_k^1 \alpha_l^1 \mathcal{E}_{ijkl} + 3\lambda_2 \sum_{j=1}^m \alpha_j^1 \mathcal{E}_{ij\lambda} = 0, \quad \sum_{i=1}^m (\alpha_i^1)^2 = 1$$

$$B_{ij} \equiv \sum_{k=1}^m \sum_{l=1}^m \alpha_k^1 \alpha_l^1 \mathcal{E}_{ijkl} + \lambda_2 \mathcal{E}_{ij\lambda}$$

Branch stable for all positive eigenvalues

$$\mathcal{E}_{ijk} \equiv ((\mathcal{E}_{,uuu}^c \overset{i}{u})\overset{j}{u})\overset{k}{u}, \quad (\mathcal{E}_{,uu}^c v_{ij} + (\mathcal{E}_{,uuu}^c \overset{i}{u})\overset{j}{u})\delta v = 0$$

$$\mathcal{E}_{ij\lambda} \equiv ((d\mathcal{E}_{,uu}/d\lambda)_c \overset{i}{u})\overset{j}{u} = ((\mathcal{E}_{,uuu}^c (d\overset{0}{u}/d\lambda)_c + \mathcal{E}_{,uu\lambda}^c) \overset{i}{u})\overset{j}{u}$$

$$\mathcal{E}_{ijkl} \equiv (((\mathcal{E}_{,uuuu}^c \overset{i}{u})\overset{j}{u})\overset{k}{u})\overset{l}{u} + (\mathcal{E}_{,uuu}^c v_{jk})\overset{l}{u} + (\mathcal{E}_{,uuu}^c v_{kl})\overset{j}{u} + (\mathcal{E}_{,uuu}^c v_{lj})\overset{k}{u}\overset{i}{u}$$



STABILITY OF CONTINUA AND NUMERICAL (FEM) METHODS

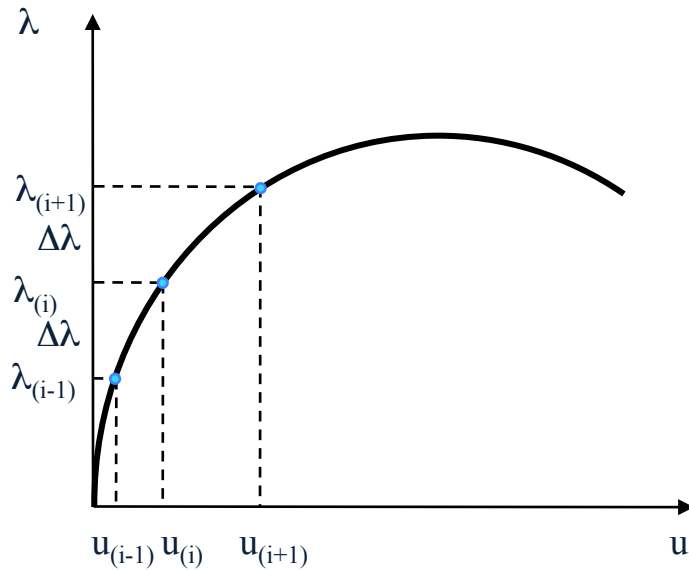


NUMERICAL (FEM) TECHNIQUES IN STABILITY PROBLEMS

- Using the Finite Element Method (FEM), problem's principal solution at load λ is obtained using an **incremental Newton-Raphson** algorithm. Method, which **starts** from **zero load – zero displacement**, always converges for **adequately small** load step $\Delta\lambda$ and gives equilibrium solution to **any accuracy** required.
- At any given load λ , **method automatically calculates** corresponding **stability operator**, which is the **tangent stiffness matrix $K(\lambda)$** .
- Solution technique uses $K = LDU$ (Cholesky) decomposition. Presence of **critical points** (i.e. limit load/bifurcation point) on the principal solution imply **zeros** in the diagonal matrix D (i.e. $(D_{ii})_{\min}(\lambda_c) = 0$).
- **Bisection** method is used to **accurately find** the critical load.
- If the critical load is an m -tuple **bifurcation point**, the m lowest entries of D are zero at the critical load.
- If the critical load is a **limit point**, **arc-length continuation** methods are used to go past this point.

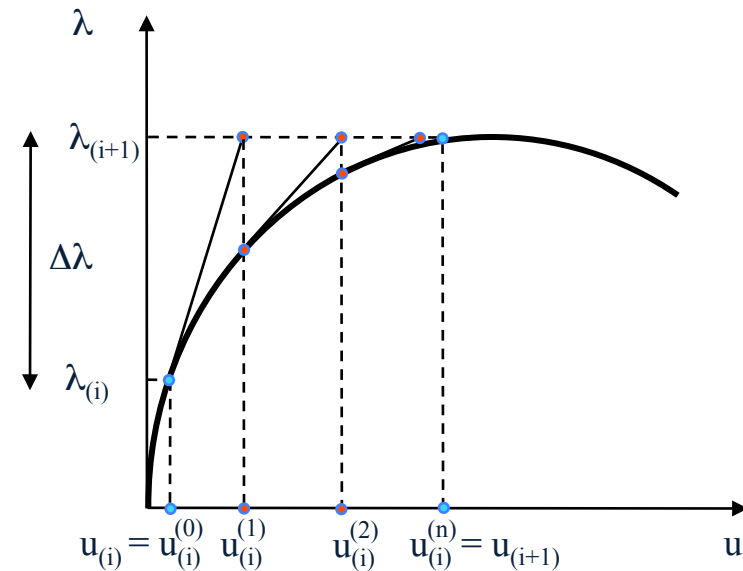


INCREMENTAL NEWTON-RAPHSON METHOD



Equilibrium solutions (principal/ bifurcated) of continuum problems amenable to finite d.o.f. case through discretization techniques (FEM)

Incremental method starting from zero load/displacement is needed to guarantee convergence of N-R (for small enough load steps)



N-R method finds equilibrium solutions and stability operator K .

$K=LDU$ decomposition of stability operator – available as part of the solution procedure – in combination with bisection gives critical points

LSK asymptotics used to start bifurcated paths



FEM DISCRETIZATION OF NONLINEAR EQUILIBRIUM

$\mathcal{E}(u, \lambda)$: continuum energy at displacement $u(\mathbf{x}) \in U$ and load $\lambda \geq 0$

$\mathcal{E}(\mathbf{u}, \lambda)$: discretized energy at displacement $\mathbf{u} \in \mathbb{R}^n$ and load $\lambda \geq 0$

$\mathbf{u} = \{u_i\}_{i=1}^n$: $u(\mathbf{x}) = \sum_{i=1}^n u_i \varphi_i(\mathbf{x})$, u_i : d.o.f, $\varphi_i(\mathbf{x}) \in U$: basis function

F.E.M. method : $\varphi_i(\mathbf{x})$ have compact support, by using element shape functions

ADVANTAGE : $\mathcal{E}_{,\mathbf{u}\mathbf{u}}$ is banded matrix, i.e. populated about its diagonal

$\mathcal{E}_{,\mathbf{u}}(\mathbf{u}, \lambda) = \mathbf{0}$: $\partial \mathcal{E} / \partial u_i = 0$, $i = 1 \dots n$: equilibrium equations

Start at : $\lambda = 0$, $\mathbf{u} = \mathbf{0}$

Continue by : Incremental Newton – Raphson Method



INCREMENTAL NEWTON-RAPHSON METHOD

Newton – Raphson method : $\mathbf{0} = \mathcal{E}_{,\mathbf{u}}(\mathbf{u} + \Delta\mathbf{u}, \lambda) \approx \mathcal{E}_{,\mathbf{u}}(\mathbf{u}, \lambda) + \mathcal{E}_{,\mathbf{u}\mathbf{u}}(\mathbf{u}, \lambda)\Delta\mathbf{u} \implies$

$$\mathbf{u}_{(i)}^{(1)} - \mathbf{u}_{(i)}^{(0)} = -[\mathcal{E}_{,\mathbf{u}\mathbf{u}}(\mathbf{u}_{(i)}^{(0)}, \lambda_{(i)})]^{-1} \mathcal{E}_{,\mathbf{u}}(\mathbf{u}_{(i)}^{(0)}, \lambda_{(i+1)}),$$

start at $\mathbf{u}_{(i)}^{(0)} = \mathbf{u}_{(i)} \equiv \mathbf{u}(\lambda_{(i)})$, where $\mathbf{u}_{(i)}^{(j)}$: \mathbf{u} at increment (i) and iteration (j)

$$\mathbf{u}_{(i)}^{(j+1)} - \mathbf{u}_{(i)}^{(j)} = -[\mathcal{E}_{,\mathbf{u}\mathbf{u}}(\mathbf{u}_{(i)}^{(j)}, \lambda_{(i+1)})]^{-1} \mathcal{E}_{,\mathbf{u}}(\mathbf{u}_{(i)}^{(j)}, \lambda_{(i+1)}),$$

end at $\mathbf{u}_{(i)}^{(j+1)} = \mathbf{u}_{(i+1)} \equiv \mathbf{u}(\lambda_{(i+1)})$, if error is small : $\|\mathcal{E}_{,\mathbf{u}}(\mathbf{u}_{(i)}^{(j)}, \lambda_{(i+1)})\| < \varepsilon$

STABILITY CHECK : positive definiteness of $\mathcal{E}_{,\mathbf{u}\mathbf{u}} = \mathbf{LDU}$ (Choleski decomposition)

\mathbf{L} : lower triangular, $\mathbf{L}^T = \mathbf{U}$: upper triangular, \mathbf{D} : diagonal, matrices

$\mathcal{E}_{,\mathbf{u}\mathbf{u}}(\mathbf{u}(\lambda), \lambda)$ positive definite at load $\lambda \iff D_{ii}(\lambda) > 0, \forall 1 \leq i \leq n$



RELATION BETWEEN STABILITY & MICROSTRUCTURE



STABILITY APPLICATIONS AT DIFFERENT SCALES

- Structural (bars, plates)
- Materials (composites, honeycomb – microstructural scale)
- Solids (phase transformation – atomistic scale)

NEW CONCEPT: **Local** (order of unit cell dimensions) vs **global** (order of overall structural dimensions) modes

NEW TOOL (for stability of **infinite**, perfectly **periodic** structures)

Bloch waves (continuum)

Phonon spectra (discrete)

Bounded solutions of differential equations with **periodic** coefficients are of the type: $u(x) = \exp(i\omega x) p(x)$ where $p(x+L) = p(x)$ (L period of coefficients)

BIG ADVANTAGE: Only the **smallest unit cell** needs to be considered in calculations

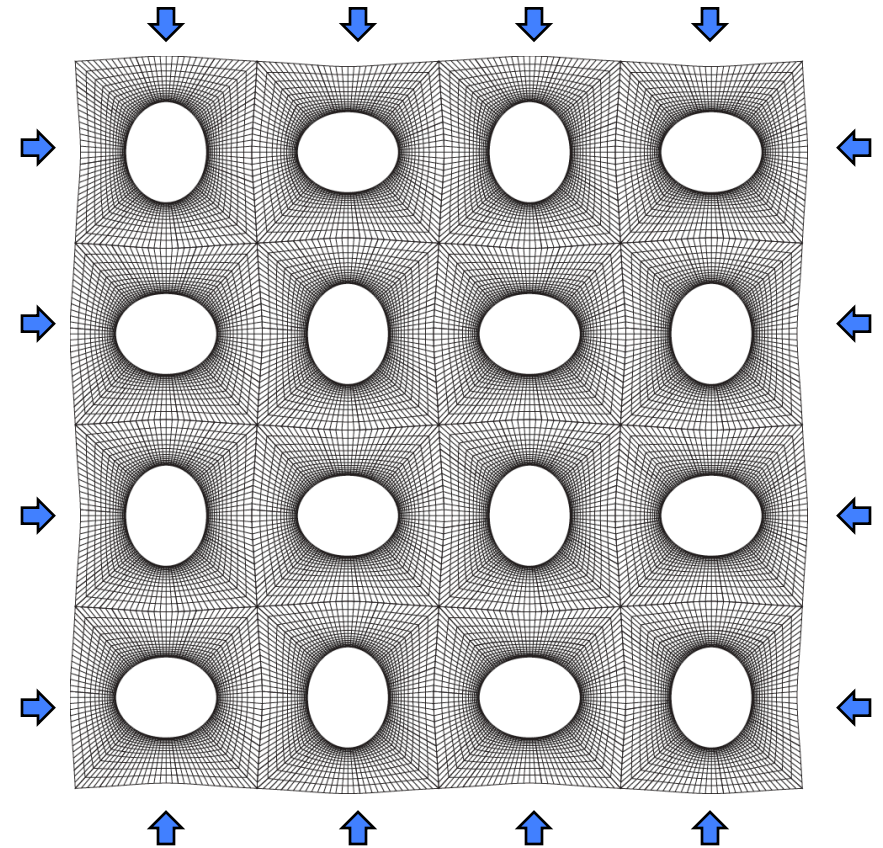
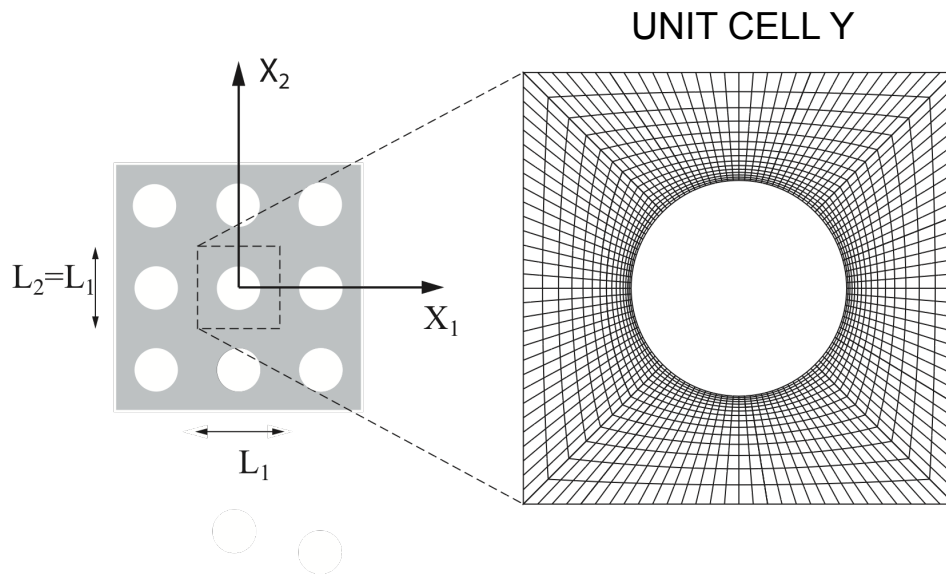


COMPRESSION-INDUCED FAILURE IN CELLULAR SOLIDS

- To model the entire deformation history of a cellular solid under compression, one has to solve for **a finite-size structure** (**boundary effects are important**) with **many unit cells**, using an **elastoplastic** constitutive law (**unloading is important**). In addition, **initial imperfections** have to be used, with **different imperfection shapes** often giving very **different results**.
- However, the **onset of the first instability** during the load increase in an **infinite, perfect structure** can be **found accurately** from the **principal solution**, by **using one unit cell**.
- The use of **only a unit cell** in finding the **first instability** occurring in a loading process is guaranteed from **Bloch wave representation** theorem for the solution of a system of linear differential equations **with periodic coefficients**. The Bloch wave representation theorem is the **generalization to PDE's** of **Floquet's theorem for ODE's** with periodic coefficients.
- The Bloch wave representation theorem is easily **adapted to cellular geometry**.
- The use of an elastic model in calculations for elastoplastic solids is based on the assumption that in the **principal solution**, **all cell walls satisfy loading condition** as load increases, thus using a **deformation theory of plasticity** (which has a stored energy).



STABILITY OF INFINITE PERIODIC SOLIDS: BLOCH WAVE



- The **Y-periodic, principal solution** of infinite, perfect solid is **initially stable**.
- Upon load increase, the system **bifurcates** with modes that are **no longer Y-periodic**.
- **Critical load** and corresponding **eigenmode** can be found based on calculations on **one unit cell Y** with the help of **Bloch wave representation theorem**.

First bifurcation mode of a porous, compressible neo-Hookean solid ($W = 0.5[\mu(I_2 - 2 - \ln I_2) + (\kappa - \mu)(\sqrt{I_2 - 1})^2]$) loaded under compressive, equi-biaxial plane strain ($E_{11} = E_{22} = -\lambda$). The critical load is $\lambda_c = 8\%$



STABILITY OF INFINITE PERIODIC SOLIDS: BLOCH WAVE

$$\beta^0(\lambda) = \min_{\delta u \in U} \left[(\mathcal{E}_{,uu}(\overset{0}{u}(\lambda), \lambda) \delta u) \delta u \right], \quad \|\delta u\| = 1; \quad \text{stability of } \overset{0}{u}(\lambda)$$

$$\overset{0}{u}(\lambda) = Y\text{-periodic (unit cell } Y) : \overset{0}{u}_{i,j}(X_k + n_k L_k) = \overset{0}{u}_{i,j}(X_k) (!); \quad n_k \in \mathbb{N}.$$

$$(\mathcal{E}_{,uu} \delta u) \delta u = \int_V \left\{ \left[\frac{\partial^2 W}{\partial F_{ij} \partial F_{kl}} \right]_{\overset{0}{u}} \delta u_{i,j} \delta u_{k,l} \right\} dV; \quad \delta u_{i,j} \equiv \partial \delta u_i / \partial X_j, \quad V = \mathbb{R}^2 \text{ or } \mathbb{R}^3$$

$$\forall \delta u \in U : \quad \delta u_j(\mathbf{X}) = \delta p_j(\mathbf{X}) \exp(i\omega_k X_k) : \text{BLOCH WAVE THEOREM.}$$

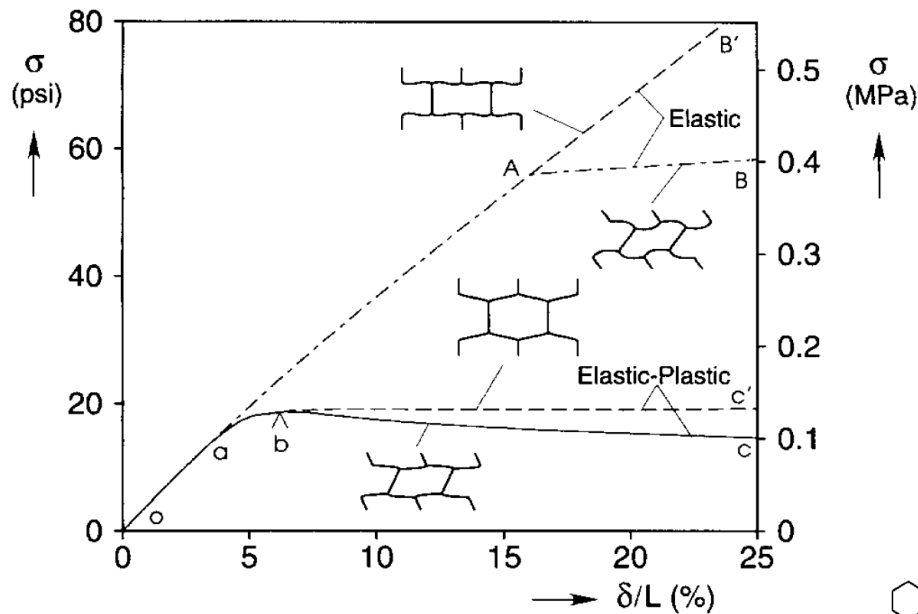
$$\text{where : } \quad \omega_k L_k (!) \in (0, 2\pi); \quad k = 1, 2 \text{ if } V = \mathbb{R}^2 \text{ or } k = 1, 2, 3 \text{ if } V = \mathbb{R}^3$$

$$\delta \mathbf{p} = Y\text{-periodic : } \quad \delta p_j(X_k + n_k L_k) = \delta p_j(X_k) (!); \quad n_k \in \mathbb{N}.$$

$$\beta^0(\lambda) = \inf_{\omega} \left[\min_{\delta \mathbf{p}} \int_Y \left\{ \left[\frac{\partial^2 W}{\partial F_{ij} \partial F_{kl}} \right]_{\overset{0}{u}} \overline{\delta u}_{i,j} \delta u_{k,l} \right\} dV \right]; \quad \text{calculations need only } Y$$



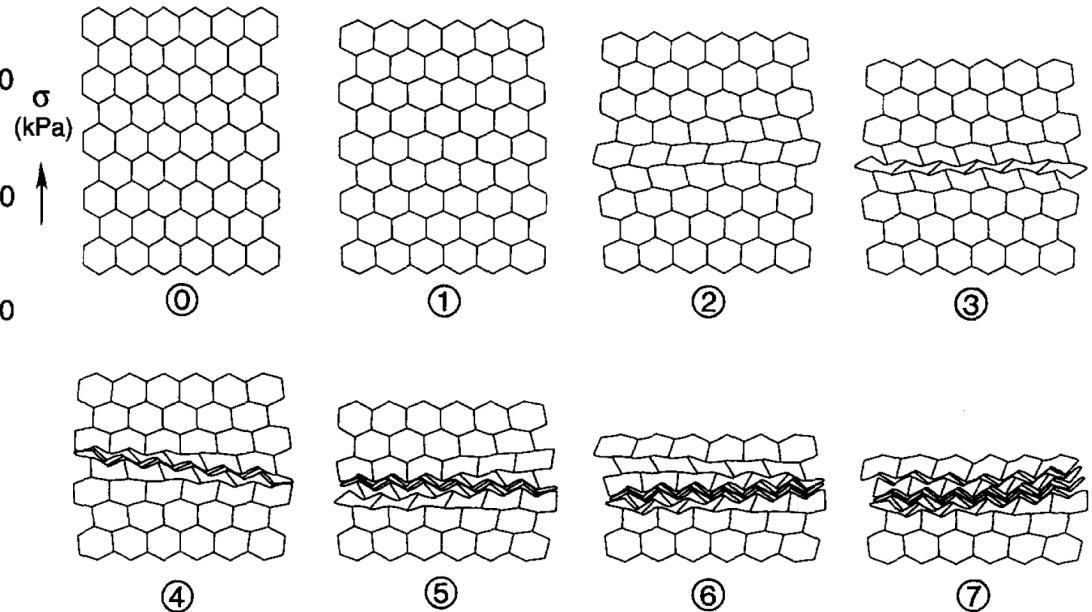
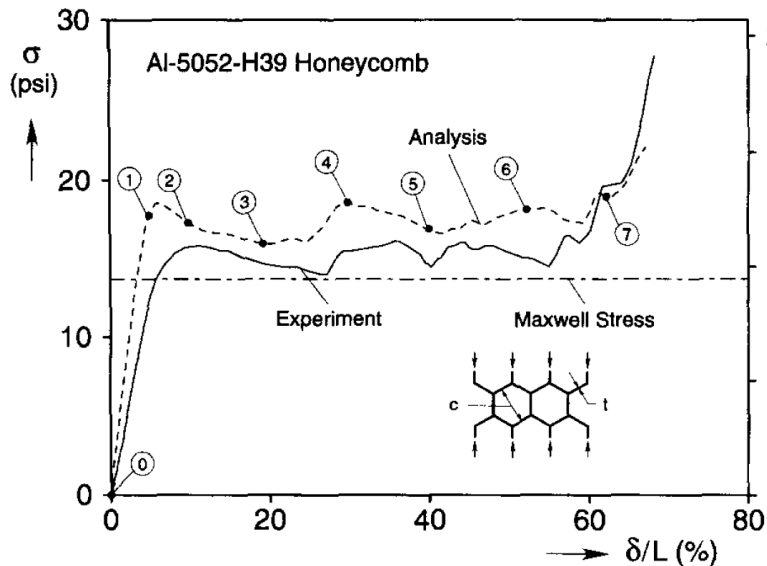
MEC 563 - STABILITY OF SOLIDS - REVIEW



Sequence of events in 2D loading of a cellular (hexagonal cells) solid:

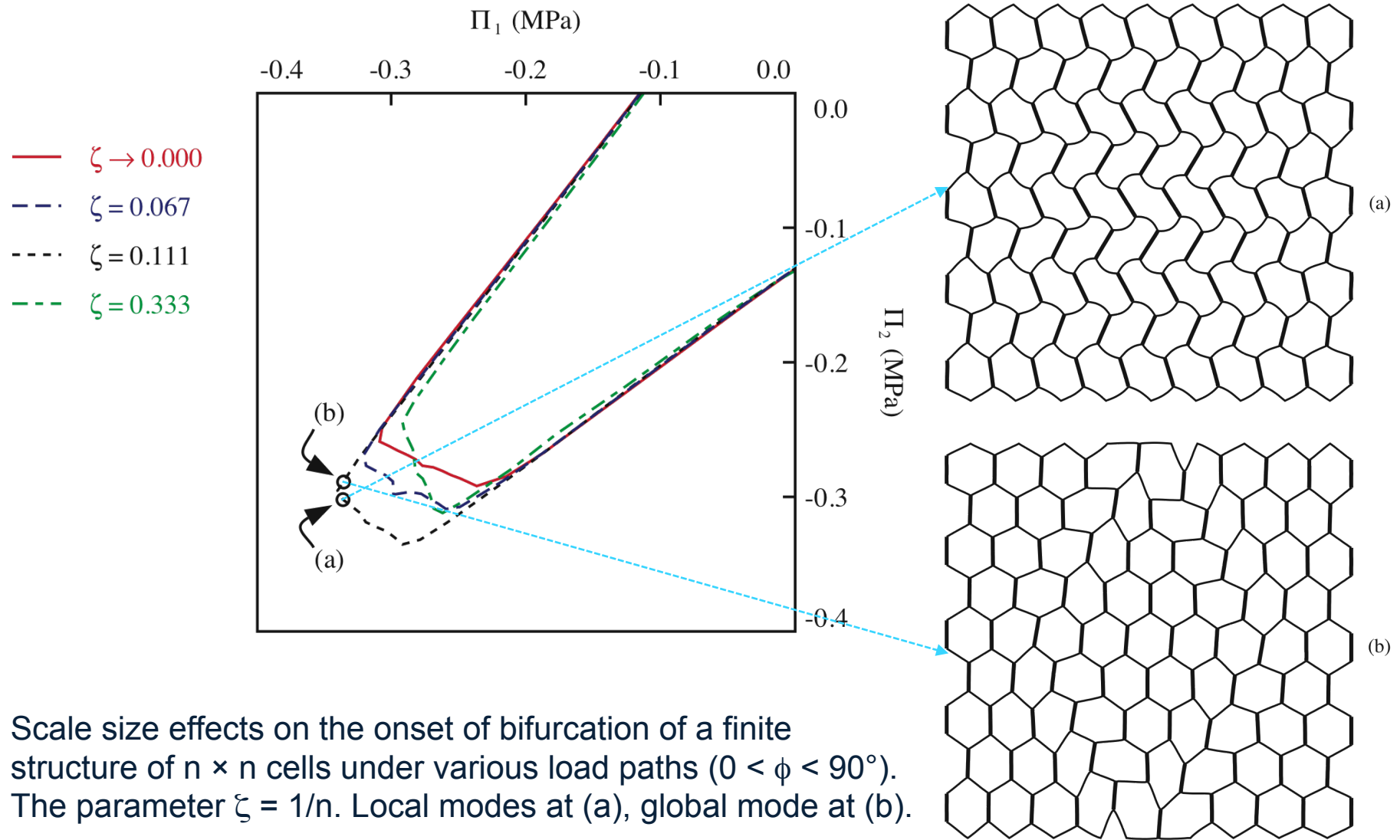
- **Initial bifurcation** (local mode, involving one row) occurs under **reduced loads**.
- Deformation **localizes in that row** until entire row collapses (contact) and the process restarts. Notice strong **boundary effects** in this experiment.

FROM: Papka & Kyriakides JMPS, 1994, 42, pp. 1499-1532





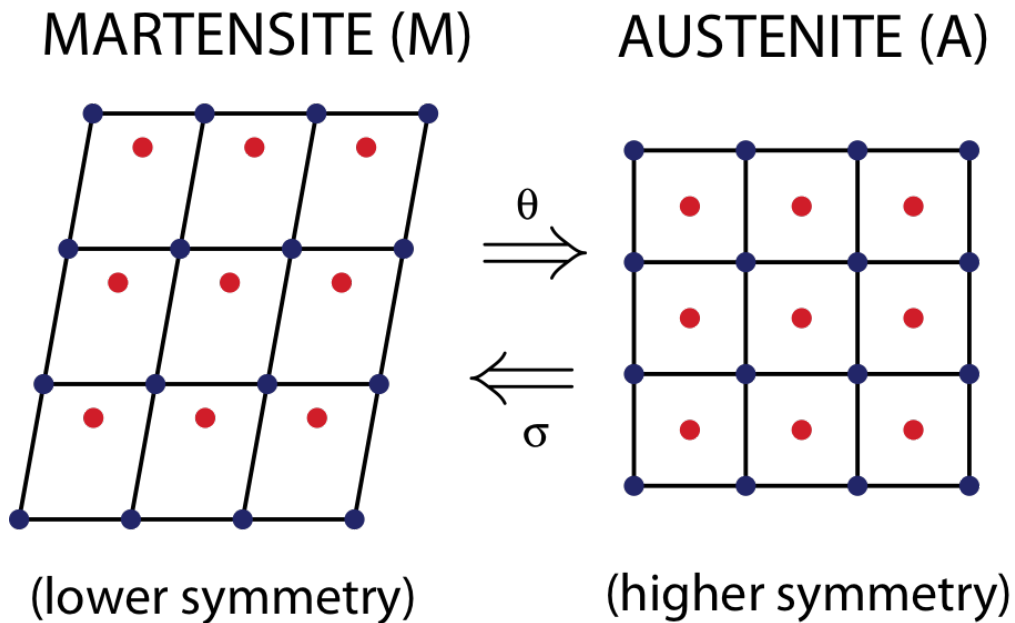
HEXAGONAL HONEYCOMB: LOCAL AND GLOBAL MODES



Scale size effects on the onset of bifurcation of a finite structure of $n \times n$ cells under various load paths ($0 < \phi < 90^\circ$). The parameter $\zeta = 1/n$. Local modes at (a), global mode at (b).



PHASE TRANSFORMATIONS: LATTICE INSTABILITIES



- **Shape memory** behavior due to **instabilities** of the **atomic lattice**:

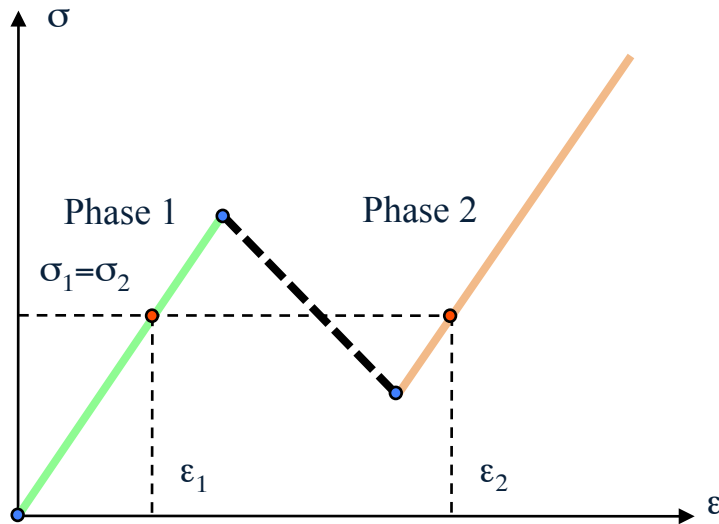
- At **higher temperatures**: **austenitic** (**higher symmetry phase**) is **stable**.

- At **higher stresses**: **martensitic** (**lower symmetry phase**) is **stable**.

- The **consequence** of this **lattice-level instability** **shows** all the way up to **structural scale**.



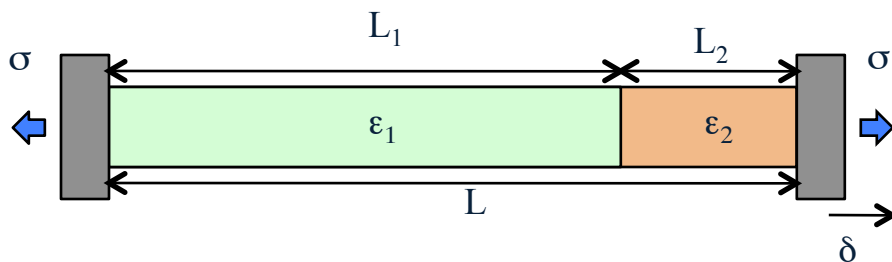
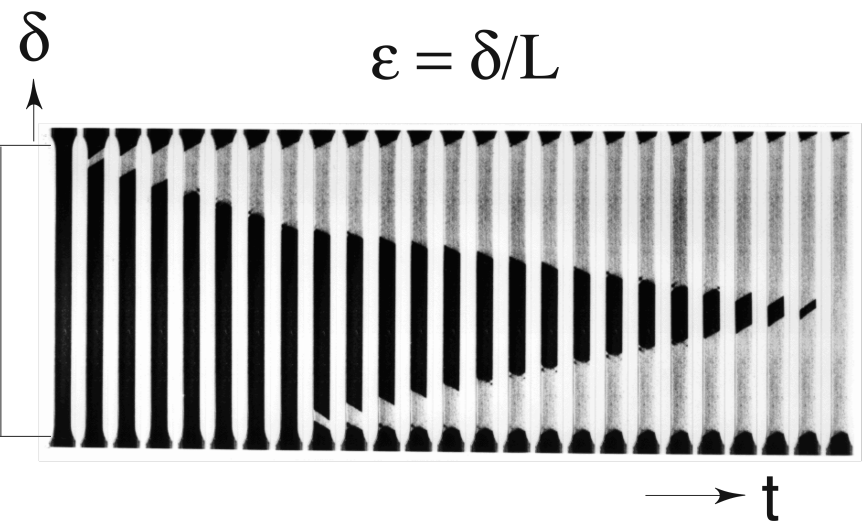
PHASE TRANSFORMATIONS: MACROSCOPIC MODELING



- Stress is **not a monotonically increasing** function of strain, due to the presence of **two different phases**.

- The solution to the uniaxial stretching strip problem has **discontinuities** and is **not unique**.

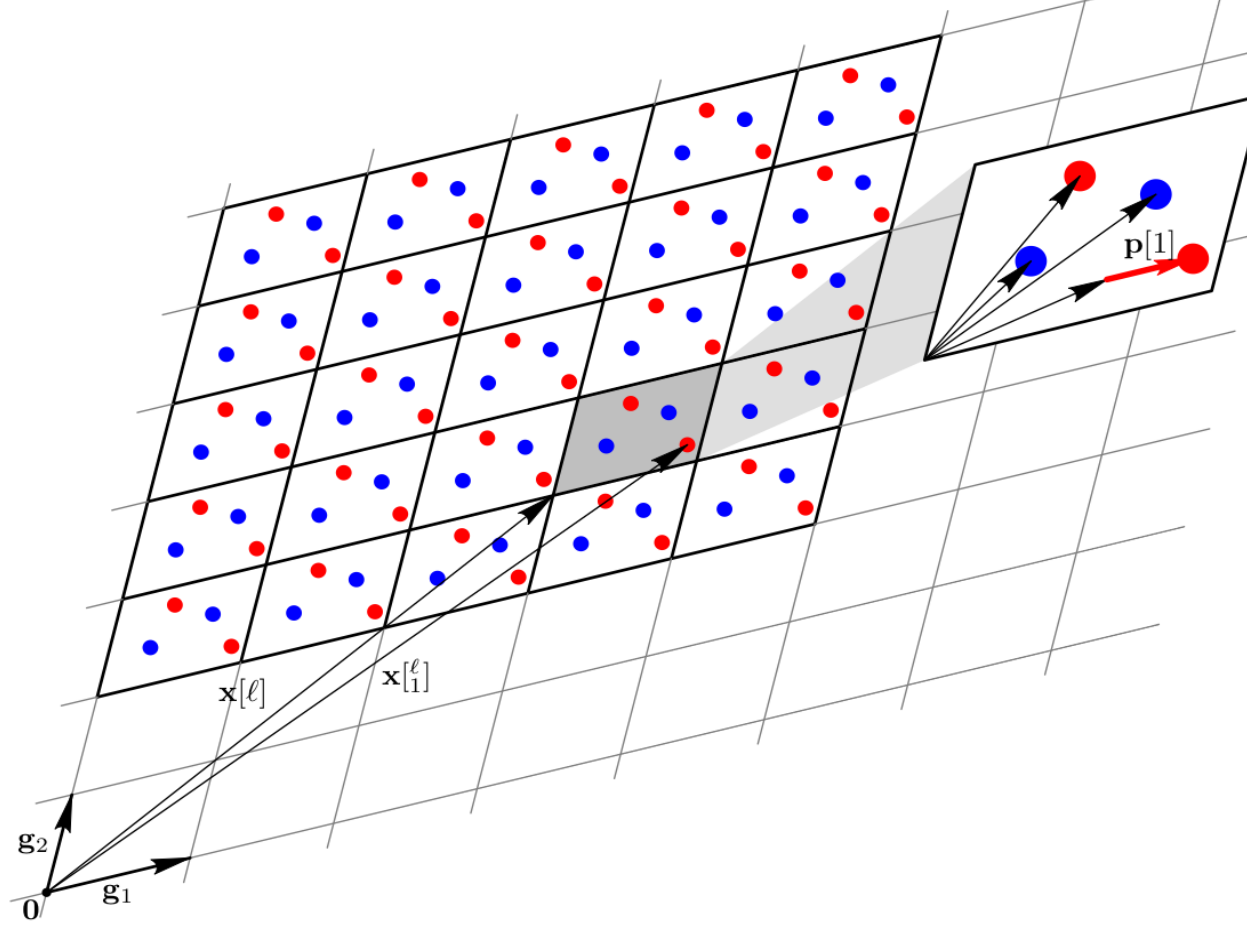
PROPAGATING INSTABILITY IN A NiTi STRIP (J. SHAW, PhD 1997)





PHASE TRANSFORMATIONS: ATOMISTIC MODELING

$$\mathbf{x} [\alpha]^\ell = \mathbf{U} \cdot (\mathbf{X} [\alpha]^\ell + \mathbf{P}[\alpha]) = \mathbf{U} \cdot \mathbf{X} [\alpha]^\ell + \mathbf{p}[\alpha]$$



$\alpha = 0, 1, 2, 3$

$\mathbf{X} [\alpha]^\ell$ – reference pos.

$S[\alpha]$ – fractional pos.

\mathbf{G}_i – ref. lattice basis

$\mathbf{X}[\ell]$ – unit-cell ref. pos.

$\mathbf{P}[\alpha]$ – sub-lat. ref. shifts

\mathbf{U} – uniform deformation

$\mathbf{x} [\alpha]^\ell$ – current pos.

$\mathbf{p}[\alpha]$ – sub-lat. current pos.

$\mathbf{x}[\ell]$ – unit-cell current pos.

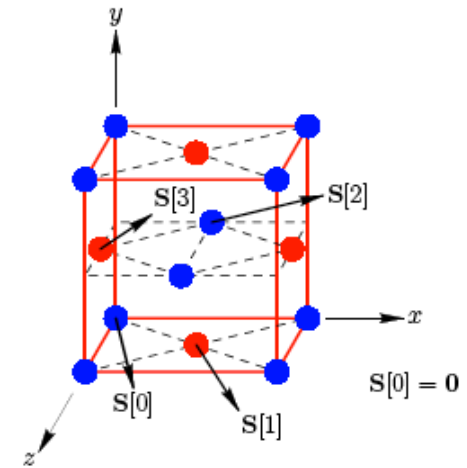
\mathbf{g}_i – current lattice basis



CAUCHY-BORN HYPOTHESIS: EQUILIBRIUM & STABILITY

- Equilibrium:

$$\frac{\partial \tilde{W}}{\partial \mathbf{u}} = 0 \left\{ \begin{array}{l} \frac{\partial \tilde{W}}{\partial \mathbf{U}} = 0, \\ \frac{\partial \tilde{W}}{\partial \mathbf{S}[1]} = 0, \quad \frac{\partial \tilde{W}}{\partial \mathbf{S}[2]} = 0, \quad \frac{\partial \tilde{W}}{\partial \mathbf{S}[3]} = 0. \end{array} \right.$$



- Stability for perturbations of ∞ wavelength):
 - Cauchy-Born stability (local energy minimizer):

$$\delta \mathbf{u} \frac{\partial^2 \tilde{W}}{\partial \mathbf{u} \partial \mathbf{u}} \delta \mathbf{u} > 0;$$

$$\delta \mathbf{u} = \{\delta \mathbf{U}, \delta \mathbf{S}[1], \delta \mathbf{S}[2], \delta \mathbf{S}[3]\}, \quad \delta \mathbf{U} = \delta \mathbf{U}^T.$$



PHONON STABILITY FOR INFINITE, PERFECT LATTICE

- Linearized equations of motion about equilibrium:

$$m_{\alpha} \ddot{\mathbf{u}} \begin{bmatrix} \ell \\ \alpha \end{bmatrix} = - \sum_{\substack{\ell' \\ \alpha'}} \mathbf{K} \begin{bmatrix} \ell & \ell' \\ \alpha & \alpha' \end{bmatrix} \cdot \mathbf{u} \begin{bmatrix} \ell' \\ \alpha' \end{bmatrix},$$

m_{α} – mass of atom α ,

$\mathbf{u} \begin{bmatrix} \ell \\ \alpha \end{bmatrix}$ – displacement of atom α in unit cell ℓ ,

$\mathbf{K} \begin{bmatrix} \ell & \ell' \\ \alpha & \alpha' \end{bmatrix}$ – stiffness between atoms $\begin{bmatrix} \ell \\ \alpha \end{bmatrix}$ and $\begin{bmatrix} \ell' \\ \alpha' \end{bmatrix}$ calculated from the atomic potentials.

- Initial conditions:

$$\mathbf{u} \begin{bmatrix} \ell \\ \alpha \end{bmatrix} \Big|_{t=0} = \mathbf{u}^0 \begin{bmatrix} \ell \\ \alpha \end{bmatrix}, \quad \dot{\mathbf{u}} \begin{bmatrix} \ell \\ \alpha \end{bmatrix} \Big|_{t=0} = \dot{\mathbf{u}}^0 \begin{bmatrix} \ell \\ \alpha \end{bmatrix}.$$

- Stability (in the sense of Lyapunov):

$$\|\mathbf{u}^0 \begin{bmatrix} \ell \\ \alpha \end{bmatrix}\|, \|\dot{\mathbf{u}}^0 \begin{bmatrix} \ell \\ \alpha \end{bmatrix}\| < \epsilon \implies \|\mathbf{u} \begin{bmatrix} \ell \\ \alpha \end{bmatrix}\|, \|\dot{\mathbf{u}} \begin{bmatrix} \ell \\ \alpha \end{bmatrix}\| < \delta(\epsilon).$$



PHONON STABILITY FOR INFINITE, PERFECT LATTICE

- Phonon (normal mode) solutions: (a -lattice spacing, $M = 4$ -atoms/unit-cell)

$$\mathbf{u} \begin{bmatrix} \ell \\ \alpha \end{bmatrix} = \Delta \mathbf{u}^{(q)}[\alpha] \exp \left\{ -i \left(\mathbf{k} \cdot \mathbf{X} \begin{bmatrix} \ell \\ \alpha \end{bmatrix} + \omega^{(q)}(\mathbf{k})t \right) \right\},$$

\mathbf{k} – wave number vector, $\mathbf{k} \in \left[-\frac{\pi}{a}, \frac{\pi}{a} \right)^3$;

q – phonon index, $q = 1, 2, \dots, 3M$;

$\omega^{(q)}(\mathbf{k})$ – phonon frequency;

$\Delta \mathbf{u}^{(q)}[\alpha]$ – amplitude vector.

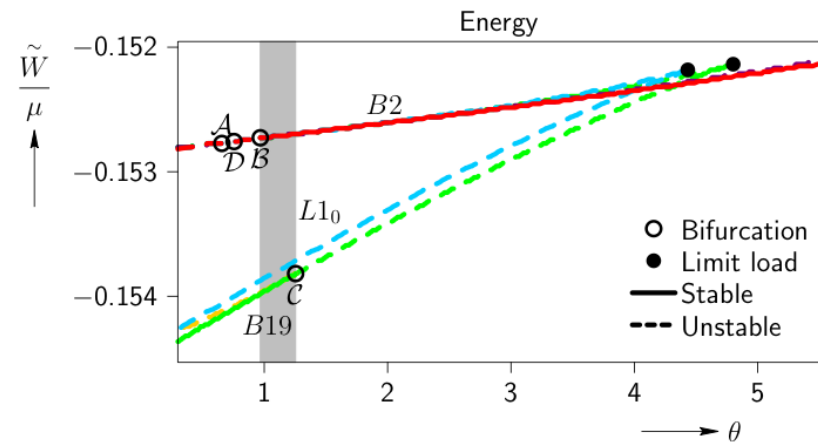
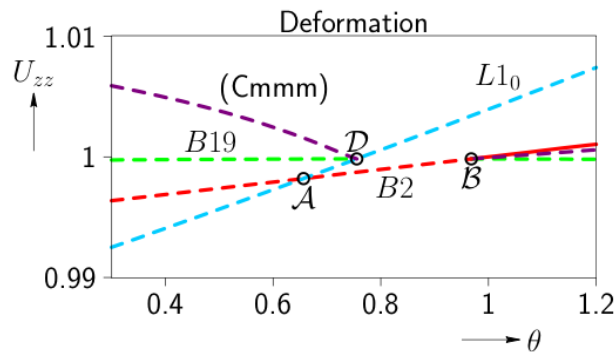
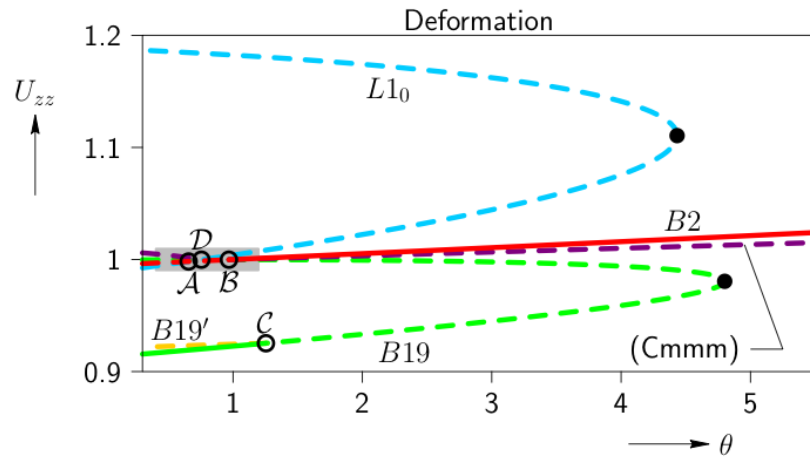
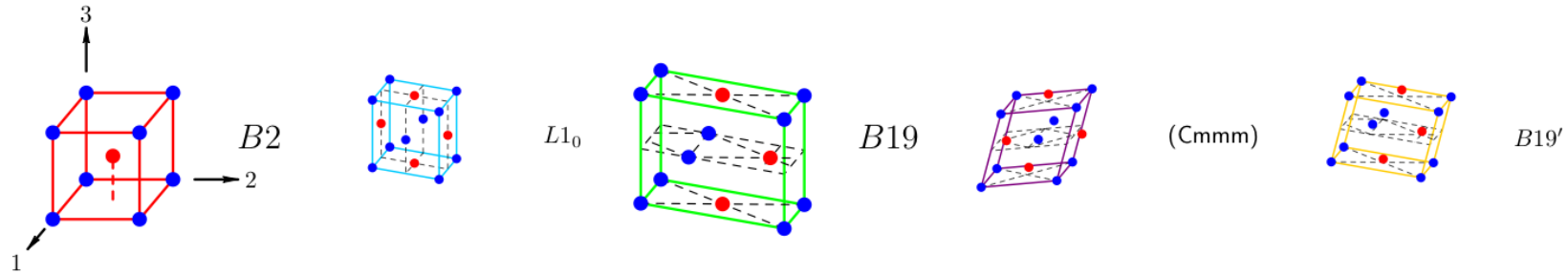
- Phonon-stability:

$$\left(\omega^{(q)}(\mathbf{k}) \right)^2 > 0, \text{ for all } \mathbf{k}, \text{ and all } q.$$

PHONON STABILITY FOR DISCRETE SYSTEMS IS SAME TO BLOCH WAVE FOR CONTINUA



PHONON STABILITY FOR INFINITE, PERFECT LATTICE





SOME FINAL COMMENTS

- **Thank you for taking class and following up especially for my morning lecture devotees**
- **Hope key concepts & new ideas from this class remain with you long after details forgotten**
- **Encourage you to stop by with questions, comments and suggestions on how to improve class**
- **My office door wide open for those of you interested in this area and willing to learn more – I am welcoming you to do research in this area (and a thesis if interested...)**