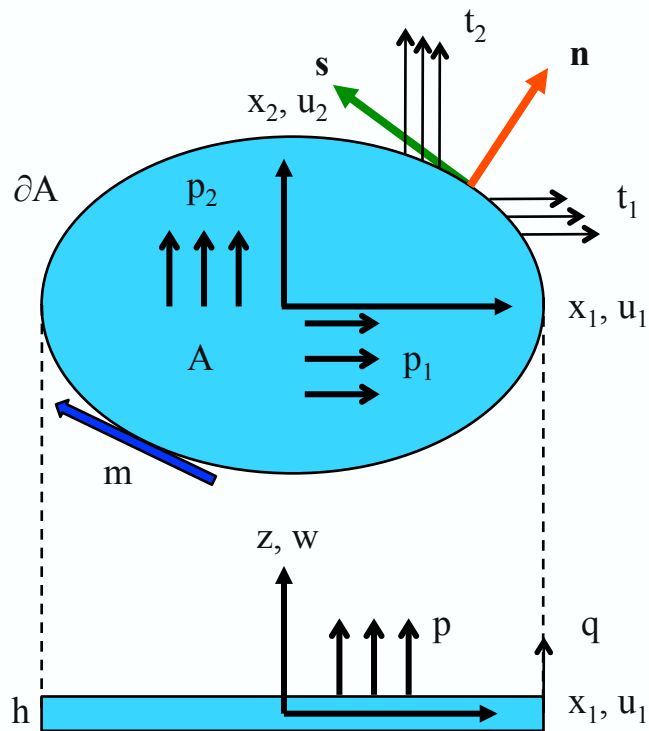




VON KARMAN PLATE – ASSUMPTIONS

Assumptions:



- Small strains
- Plane stress state
- Linearly elastic response
- Linear strain distribution through thickness
- Normals to mid-plane stay normal after deformation
- Moderate in-plane rotations of mid-plane



EXAMPLE - II – SIMPLE MODE



VON KARMAN PLATE – KINEMATICS & CONSTITUTIVE LAW

$$\text{Plane stress state : } \sigma_{\alpha\beta}(x_1, x_2, z) = L_{\alpha\beta\gamma\delta}\varepsilon_{\gamma\delta}(x_1, x_2, z); \quad (\text{Greek indexes : } 1, 2)$$

$$\text{Plane stress moduli : } L_{\alpha\beta\gamma\delta} = \frac{E}{1-\nu^2} \left[\frac{1-\nu}{2} (\delta_{\alpha\gamma}\delta_{\beta\delta} + \delta_{\alpha\delta}\delta_{\beta\gamma}) + \nu\delta_{\alpha\beta}\delta_{\gamma\delta} \right]$$

$$\text{Strain distribution : } \varepsilon_{\alpha\beta}(x_1, x_2, z) = E_{\alpha\beta}(x_1, x_2) + zK_{\alpha\beta}(x_1, x_2)$$

$$\text{Membrane strains : } E_{\alpha\beta} = \frac{1}{2}(u_{\alpha,\beta} + u_{\beta,\alpha}) + \frac{1}{2}w_{,\alpha}w_{,\beta}; \quad (f_{,\alpha} \equiv \partial f / \partial x_\alpha)$$

$$\text{Curvature strains : } K_{\alpha\beta} = -w_{,\alpha\beta}$$

$$\text{Membrane resultants : } N_{\alpha\beta} = \int_{-h/2}^{h/2} \sigma_{\alpha\beta} dz = hL_{\alpha\beta\gamma\delta}E_{\gamma\delta}$$

$$\text{Moment resultants : } M_{\alpha\beta} = \int_{-h/2}^{h/2} \sigma_{\alpha\beta} z dz = \frac{h^3}{12}L_{\alpha\beta\gamma\delta}K_{\gamma\delta}$$



EXAMPLE - II – SIMPLE MODE



VON KARMAN PLATE – ENERGY

$$\text{Internal energy : } \mathcal{E}_{int} = \int_A \left[\frac{1}{2} N_{\alpha\beta} E_{\alpha\beta} + \frac{1}{2} M_{\alpha\beta} K_{\alpha\beta} \right] h dA$$

$$\text{External energy : } \mathcal{E}_{ext} = - \int_A [p_\alpha u_\alpha + pw] dA - \int_{\partial A} [t_\alpha u_\alpha + qw + m(-w_{,n})] ds$$

$$\text{Total energy : } \mathcal{E} = \mathcal{E}_{int} + \mathcal{E}_{ext}$$

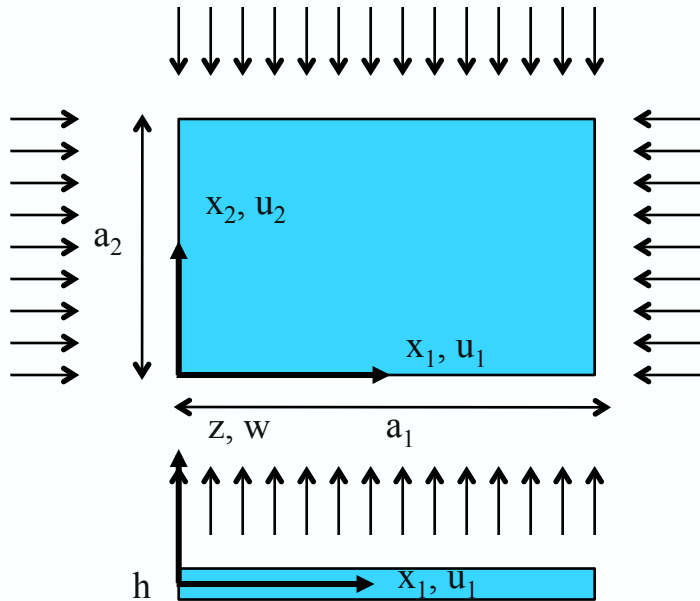
$$\begin{aligned} \mathcal{E} = & \frac{1}{2} \int_A \left[L_{\alpha\beta\gamma\delta} (E_{\alpha\beta} E_{\gamma\delta} + \frac{h^2}{12} K_{\alpha\beta} K_{\gamma\delta}) h \right] dA - \\ & - \int_A [p_\alpha u_\alpha + pw] dA - \int_{\partial A} [t_\alpha u_\alpha + qw + m(-w_{,n})] ds \end{aligned}$$



EXAMPLE - II – SIMPLE MODE



PLATE BUCKLING EXAMPLE – PROBLEM SETTING



$$\mathcal{E}_{ext} = - \int_{\partial A} [t_\alpha u_\alpha] ds; \quad (p_\alpha = p = q = m = 0)$$

$$t_\alpha = n_\beta \lambda \sigma_{\alpha\beta}^0 h; \quad (\text{prestress} : \lambda \sigma_{\alpha\beta}^0)$$

$$\mathcal{E}_{ext} = -\lambda \int_A [\sigma_{\alpha\beta}^0 u_{\alpha,\beta}] h dA,$$

$$\mathcal{E} = \mathcal{E}_{int} + \mathcal{E}_{ext}$$

$$\mathcal{E}(u, \lambda) = \int_A \left[\frac{1}{2} L_{\alpha\beta\gamma\delta} (E_{\alpha\beta} E_{\gamma\delta} + \frac{h^2}{12} K_{\alpha\beta} K_{\gamma\delta}) - \lambda \sigma_{\alpha\beta}^0 u_{\alpha,\beta} \right] h dA, \quad u \equiv (u_1, u_2, w)$$

$$w(0, x_2) = w(a_1, x_2) = w(x_1, 0) = w(x_1, a_2) = 0; \quad (w = 0, \text{ simple support on } \partial A)$$

$$u_1(0, x_2) = u_{1,2}(a_1, x_2) = u_2(x_1, 0) = u_{2,1}(x_1, a_2) = 0; \quad (u_{\alpha,s} = 0, \text{ straight edges on } \partial A)$$



EXAMPLE - II – SIMPLE MODE



PLATE BUCKLING EXAMPLE – EQUILIBRIUM

Equilibrium equations :

$$\mathcal{E},_u \delta u = \int_A \left[L_{\alpha\beta\gamma\delta} (E_{\alpha\beta} \delta E_{\gamma\delta} + \frac{h^2}{12} K_{\alpha\beta} \delta K_{\gamma\delta}) - \lambda \sigma_{\alpha\beta}^0 \delta u_{\alpha,\beta} \right] h dA = 0$$

$$\delta E_{\alpha\beta} = \frac{1}{2} (\delta u_{\alpha,\beta} + \delta u_{\beta,\alpha}) + \frac{1}{2} (w_{,\alpha} \delta w_{,\beta} + w_{,\beta} \delta w_{,\alpha}), \quad \delta K_{\alpha\beta} = -\delta w_{,\alpha\beta}$$

Principal solution is flat plate configuration :

$$\overset{0}{N}_{\alpha\beta} = \lambda h \overset{0}{\sigma}_{\alpha\beta}, \quad (\overset{0}{\sigma}_{11}, \overset{0}{\sigma}_{22} \neq 0, \quad \overset{0}{\sigma}_{12} = \overset{0}{\sigma}_{21} = 0); \quad \overset{0}{M}_{\alpha\beta} = 0$$

$$\overset{0}{u}_1 = (\lambda x_1 / E) (\overset{0}{\sigma}_{11} - \nu \overset{0}{\sigma}_{22}), \quad \overset{0}{u}_2 = (\lambda x_2 / E) (\overset{0}{\sigma}_{22} - \nu \overset{0}{\sigma}_{11}); \quad \overset{0}{w} = 0$$



EXAMPLE - II – SIMPLE MODE



PLATE BUCKLING EXAMPLE – BIFURCATION

$$(\mathcal{E}^c,_{uu} \overset{1}{u}) \delta u = \int_A \left[L_{\alpha\beta\gamma\delta} (\overset{1}{u}_{\alpha,\beta} \delta u_{\gamma,\delta} + \frac{h^2}{12} \overset{1}{w}_{,\alpha\beta} \delta w_{,\gamma\delta}) + \lambda \overset{0}{\sigma}_{\alpha\beta} \overset{1}{w}_{,\alpha} \delta w_{,\beta} \right] h dA = 0$$

Integration by parts gives following Euler – Lagrange system ($\overset{1}{u} \equiv (\overset{1}{u}_1, \overset{1}{u}_2, \overset{1}{w})$)

$$\delta u_\alpha : \quad (L_{\alpha\beta\gamma\delta} \overset{1}{u}_{\gamma,\delta}),_{\beta} = 0 \text{ in } A,$$

$$L_{12\gamma\delta} \overset{1}{u}_{\gamma,\delta} = 0 \text{ on } \partial A, \quad \overset{1}{u}_1(0, x_2) = \overset{1}{u}_{1,2}(a_1, x_2) = \overset{1}{u}_2(x_1, 0) = \overset{1}{u}_{2,1}(x_1, a_2) = 0,$$

$$\text{Solution : } \overset{1}{u}_\alpha = 0$$

$$\delta w : \quad (h^2/12) L_{\alpha\beta\gamma\delta} \overset{1}{w}_{,\alpha\beta\gamma\delta} - \lambda \overset{0}{\sigma}_{\alpha\beta} \overset{1}{w}_{,\alpha\beta} = 0 \text{ in } A,$$

$$\overset{1}{w} = 0 \text{ on } : \partial A : \quad \overset{1}{w}_{,11}(0, x_2) = \overset{1}{w}_{,11}(a_1, x_2) = \overset{1}{w}_{,22}(x_1, 0) = \overset{1}{w}_{,22}(x_1, a_2) = 0$$

$$\text{Solution : } \overset{1}{w} = h \sin(m\pi x_1/a_1) \sin(n\pi x_2/a_2)$$



EXAMPLE - II – SIMPLE MODE



PLATE BUCKLING EXAMPLE – BIFURCATION

$$\mathcal{E}^c_{,u\lambda} \overset{1}{u} = - \int_A [\overset{0}{\sigma}_{\alpha\beta} \overset{1}{u}_{\alpha,\beta}] h dA = 0 \implies \text{Bifurcation}$$

$$\lambda_c = \frac{Eh^2}{12(1-\nu^2)} \min_{m,n \in \mathbb{N}} \left\{ - \frac{[(m\pi/a_1)^2 + (n\pi/a_2)^2]^2}{\overset{0}{\sigma}_{11}(m\pi/a_1)^2 + \overset{0}{\sigma}_{22}(n\pi/a_2)^2} \right\} : \text{Critical load}$$

$\overset{0}{\sigma}_{11}(m\pi/a_1)^2 + \overset{0}{\sigma}_{22}(n\pi/a_2)^2 < 0$ at least one stress component compressive

(m_c, n_c) at λ_c : depend on geometry – not unique pair necessarily

(m_c, n_c) at λ_c : unique pair \implies simple bifurcation



EXAMPLE - II – SIMPLE MODE



PLATE BUCKLING EXAMPLE – PRINCIPAL PATH STABILITY

$$(\mathcal{E},_{uu} (\overset{0}{u}(\lambda), \lambda)\delta u)\delta u = \int_A \left[L_{\alpha\beta\gamma\delta}(\delta u_{\alpha,\beta}\delta u_{\gamma,\delta} + \frac{h^2}{12}\delta w_{,\alpha\beta}\delta w_{,\gamma\delta}) + \lambda\overset{0}{\sigma}_{\alpha\beta}\delta w_{,\alpha}\delta w_{,\beta} \right] hdA$$

$$\delta w = h \sum_{n=1}^{\infty} \sum_{m=1}^{\infty} \delta w_{mn} \sin(m\pi x_1/a_1) \sin(n\pi x_2/a_2) : \text{Fourier representation of arbitrary } \delta w$$

$$\begin{aligned} (\mathcal{E},_{uu}^0)\delta u)\delta u &= \int_A \left[\frac{h^2}{12} L_{\alpha\beta\gamma\delta} \delta w_{,\alpha\beta} \delta w_{,\gamma\delta} + \lambda \overset{0}{\sigma}_{\alpha\beta} \delta w_{,\alpha} \delta w_{,\beta} \right] hdA = \frac{a_1 a_2 h^3}{4} \frac{Eh^2}{12(1-\nu^2)} \times \\ &\times \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} (\delta w_{mn})^2 \left[\left\{ \frac{[(m\pi/a_1)^2 + (n\pi/a_2)^2]^2}{-\overset{0}{\sigma}_{11}(m\pi/a_1)^2 - \overset{0}{\sigma}_{22}(n\pi/a_2)^2} \right\} - \lambda \right] \left[-\overset{0}{\sigma}_{11} \left(\frac{m\pi}{a_1} \right)^2 - \overset{0}{\sigma}_{22} \left(\frac{n\pi}{a_2} \right)^2 \right] \end{aligned}$$

$\lambda \in [0, \lambda_c) \implies (\mathcal{E},_{uu}^0)\delta u)\delta u > 0 \implies$ principal path is stable for loads below λ_c



EXAMPLE - II – SIMPLE MODE



PLATE BUCKLING EXAMPLE – POSTBUCKLING

$$((\mathcal{E}^c,_{uuu} \overset{1}{u}) \overset{1}{u}) \overset{1}{u} = \int_A 3[L_{\alpha\beta\gamma\delta}(\overset{1}{w}_{,\alpha} \overset{1}{w}_{,\beta} \overset{1}{u}_{\gamma,\delta})] h dA = 0 \implies \text{symmetric bifurcation}$$

$$\begin{aligned} ((\mathcal{E}^c,_{uuu} \overset{1}{u}) \overset{1}{u} + \mathcal{E}^c,_{uu} v_{\xi\xi}) \delta v &= \int_A [L_{\alpha\beta\gamma\delta}(\overset{1}{w}_{,\gamma} \overset{1}{w}_{,\delta} \delta u_{\alpha,\beta} + 2\overset{1}{u}_{\gamma,\delta} \overset{1}{w}_{,\alpha} \delta w_{,\beta})] h dA \\ + \int_A L_{\alpha\beta\gamma\delta}(\overset{2}{u}_{\gamma,\delta} \delta u_{\alpha,\beta} + \frac{h^2}{12} \overset{2}{w}_{,\gamma\delta} \delta w_{,\alpha\beta}) + \lambda_c \overset{0}{\sigma}_{\alpha\beta} \overset{2}{w}_{,\alpha} \delta w_{,\beta} &] h dA = 0 \end{aligned}$$

Integration by parts gives following Euler – Lagrange system ($v_{\xi\xi} \equiv (\overset{2}{u}_1, \overset{2}{u}_2, \overset{2}{w})$)

$$\delta u_{\alpha} : (L_{\alpha\beta\gamma\delta}(\overset{2}{u}_{\gamma,\delta} + \overset{1}{w}_{,\gamma} \overset{1}{w}_{,\delta})),_{\beta} = 0 \text{ in } A;$$

$$L_{12\gamma\delta}(\overset{2}{u}_{\gamma,\delta} + \overset{1}{w}_{,\gamma} \overset{1}{w}_{,\delta}) = 0 \text{ on } \partial A, \quad \overset{2}{u}_1(0, x_2) = \overset{2}{u}_{1,2}(a_1, x_2) = \overset{2}{u}_2(x_1, 0) = \overset{2}{u}_{2,1}(x_1, a_2) = 0$$

$$\delta w : (h^2/12)L_{\alpha\beta\gamma\delta} \overset{2}{w}_{,\alpha\beta\gamma\delta} - \lambda_c \overset{0}{\sigma}_{\alpha\beta} \overset{2}{w}_{,\alpha\beta} = 0 \text{ in } A;$$

$$\overset{2}{w} = 0 \text{ on } \partial A, \quad \overset{2}{w}_{,11}(0, x_2) = \overset{2}{w}_{,11}(a_1, x_2) = \overset{2}{w}_{,22}(x_1, 0) = \overset{2}{w}_{,22}(x_1, a_2) = 0$$



EXAMPLE - II – SIMPLE MODE



PLATE BUCKLING EXAMPLE – POSTBUCKLING

Uniqueness of eigenmode $\implies \ddot{w} = 0$

Introduce Airy function f : $s_{11} \equiv f_{,22}$, $s_{22} \equiv f_{,11}$, $s_{12} = s_{21} \equiv -f_{,12}$; $(s_{\alpha\beta,\beta} = 0)$

$$s_{\alpha\beta} \equiv L_{\alpha\beta\gamma\delta}(\ddot{u}_{\gamma,\delta} + \dot{w}_{,\gamma} \dot{w}_{,\delta}) = L_{\alpha\beta\gamma\delta} e_{\gamma\delta}, \quad e_{\alpha\beta} \equiv \frac{1}{2}(\ddot{u}_{\alpha,\beta} + \ddot{u}_{\beta,\alpha}) + \dot{w}_{,\alpha} \dot{w}_{,\beta}$$

$$\text{Notice : } e_{11} = \frac{1}{E}(s_{11} - \nu s_{22}), \quad e_{22} = \frac{1}{E}(s_{22} - \nu s_{11}), \quad e_{12} = e_{21} = \frac{1 + \nu}{E} s_{12}$$

$$\text{Compatibility : } e_{11,22} + e_{22,11} - 2e_{12,12} = 2[(\dot{w}_{,12})^2 - \dot{w}_{,11} \dot{w}_{,22}] \implies$$

$$\frac{1}{E} \nabla^4 f = h^2 (m_c \pi / a_1)^2 (n_c \pi / a_2)^2 [\cos(2m_c \pi x_1 / a_1) + \cos(2n_c \pi x_2 / a_2)]$$

$$\text{Solution : } f = \frac{Eh^2}{16} \left[\frac{(n_c/a_2)^2}{(m_c/a_1)^2} \cos(2m_c \pi x_1 / a_1) + \frac{(m_c/a_1)^2}{(n_c/a_2)^2} \cos(2n_c \pi x_2 / a_2) \right]$$



EXAMPLE - II – SIMPLE MODE



PLATE BUCKLING EXAMPLE – POSTBUCKLING

from general LSK theory recall : $\lambda_2 = -\frac{1}{3} \frac{(((\mathcal{E}^c,_{uuuu} \overset{1}{u})\overset{1}{u})\overset{1}{u})\overset{1}{u} + 3((\mathcal{E}^c,_{uuu} v_{\xi\xi})\overset{1}{u})\overset{1}{u}}{((d\mathcal{E},_{uu} / d\lambda)_c \overset{1}{u})\overset{1}{u}}$

$$(((\mathcal{E}^c,_{uuuu} \overset{1}{u})\overset{1}{u})\overset{1}{u})\overset{1}{u} + 3((\mathcal{E}^c,_{uuu} v_{\xi\xi})\overset{1}{u})\overset{1}{u} = 3 \int_A [L_{\alpha\beta\gamma\delta} (\overset{2}{u}_{\gamma,\delta} + \overset{1}{w}_{,\gamma} \overset{1}{w}_{,\delta}) \overset{1}{w}_{,\alpha} \overset{1}{w}_{,\beta}] h dA =$$

$$= 3 \int_A [s_{\alpha\beta} \overset{1}{w}_{,\alpha} \overset{1}{w}_{,\beta}] h dA = \frac{3}{32} E h^5 a_1 a_2 [(m_c \pi / a_1)^4 + (n_c \pi / a_2)^4]$$

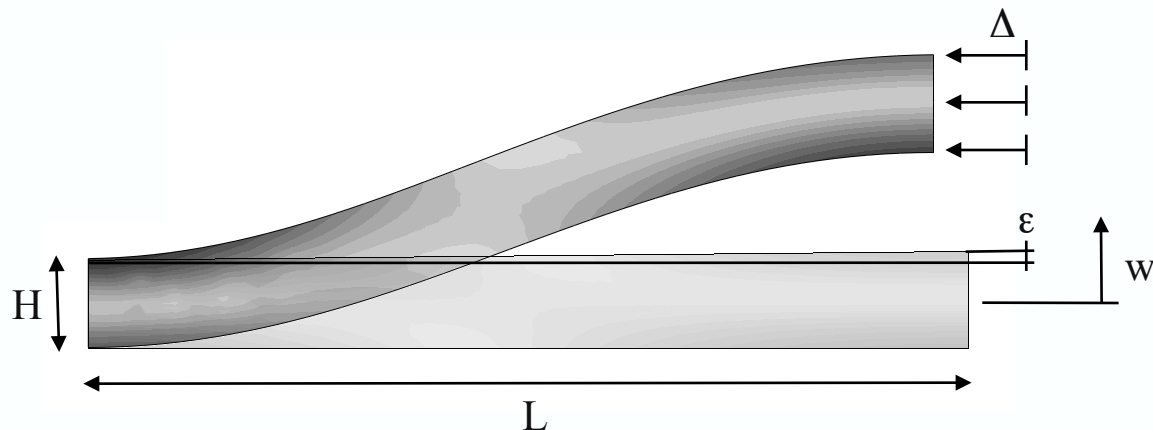
$$((d\mathcal{E},_{uu} / d\lambda)_c \overset{1}{u})\overset{1}{u} = \int_A [\overset{0}{\sigma}_{\alpha\beta} \overset{1}{w}_{,\alpha} \overset{1}{w}_{,\beta}] h dA$$

$$= \frac{h^3}{4} a_1 a_2 [\overset{0}{\sigma}_{11} (m_c \pi / a_1)^2 + \overset{0}{\sigma}_{22} (n_c \pi / a_2)^2] < 0$$

$$\lambda_2 = -\frac{E h^2}{8} \frac{(m_c \pi / a_1)^4 + (n_c \pi / a_2)^4}{\overset{0}{\sigma}_{11} (m_c \pi / a_1)^2 + \overset{0}{\sigma}_{22} (n_c \pi / a_2)^2} = \frac{3}{2} \lambda_c (1 - \nu^2) \frac{(m_c \pi / a_1)^4 + (n_c \pi / a_2)^4}{[(m_c \pi / a_1)^2 + (n_c \pi / a_2)^2]^2} > 0$$

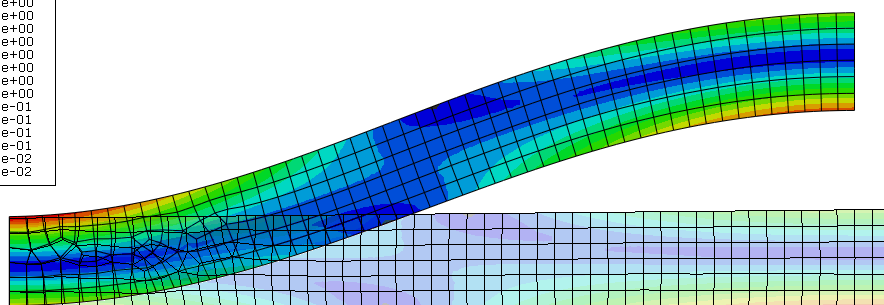
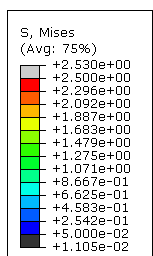


CONCEPT OF IMPERFECTION – ILLUSTRATION



Beam slenderness: $L/H = 10$

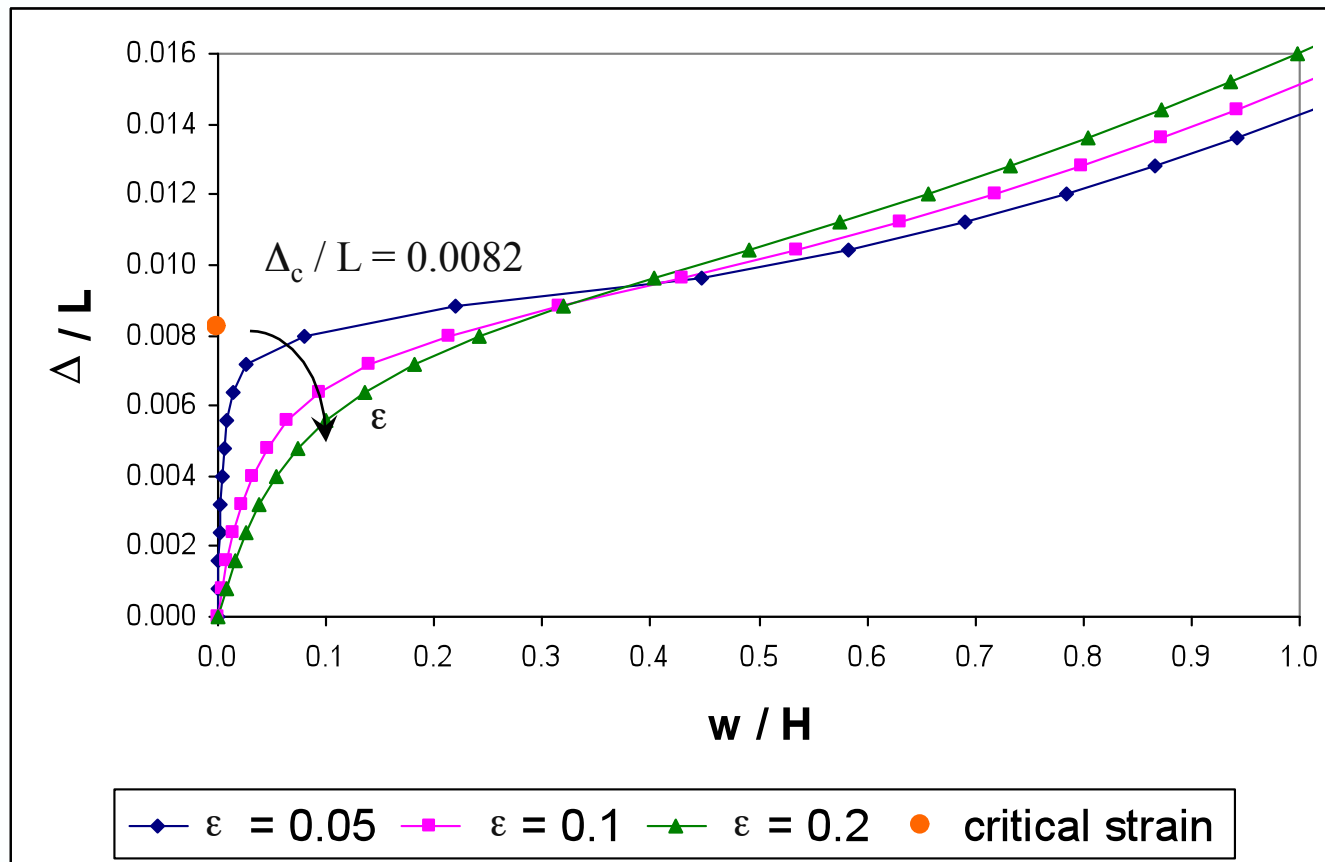
Imperfection $\varepsilon = \Delta H/H$



Deformation of an axially compressed beam that has a slight geometric imperfection (beam is trapezoidal with an imperfection angle $\varepsilon = \Delta H/H$)



CONCEPT OF IMPERFECTION – ILLUSTRATION



As imperfection amplitude ϵ decreases, equilibrium approaches perfect case



LSK ASYMPTOTICS – IMPERFECT CASE – RESULTS

- Behavior of imperfect structure near critical load can be analyzed by asymptotic expansion of equilibrium solution, just like in the perfect case
- IDEA: Study the **projection** of equilibrium solution along the (one-dimensional) null space of the **perfect** system's stability operator about its critical point
- Method finds (for a given imperfection shape) the relation at equilibrium between imperfection amplitude ε , distance from critical load $\Delta\lambda$ and projection ξ along eigenmode
- Method determines the limit points (where stability changes) of imperfect structures and the load drop $\Delta\lambda_s$ from the critical load of the perfect structure λ_c to the maximum load of the imperfect one λ_s
- **NOTE:** Imperfection can occur in **any property** (material or geometric) that **destroys** the **symmetry** of the system
- **NOTE:** By introducing concept of **imperfection amplitude** ε (scalar quantity) only **one extra** parameter is introduced in the asymptotic expansions



LSK ASYMPTOTICS – IMPERFECT CASE – EQUILIBRIUM

$\bar{\mathcal{E}}(u, \lambda, w)$: imperfect system's energy; $u(\mathbf{x}) \in U, w(\mathbf{x}) \in W$ ($w(\mathbf{x})$: imperfection),

$\bar{\mathcal{E}}(u, \lambda, 0) = \mathcal{E}(u, \lambda)$: reduces to perfect system's energy when imperfection $w(\mathbf{x}) = 0$,

$\bar{\mathcal{E}}(0, \lambda, w) = 0$: zero energy when displacement $u(\mathbf{x}) = 0$.

$\epsilon \equiv \| w \|$: imperfection amplitude; $\bar{w}(\mathbf{x}) \equiv w(\mathbf{x})/\epsilon$: imperfection shape ($\| \bar{w} \| = 1$).

$\bar{\mathcal{E}}_{,u}(u, \lambda, w)\delta u = 0$: equilibrium of imperfect system

$\bar{\mathcal{E}}_{,u}(u(\lambda, w), \lambda, w)\delta u = 0, u(\lambda, w)$: solution through $\lambda = 0$; $u(0, w) = 0, u(\lambda, 0) = \overset{0}{u}(\lambda)$

NOTE: Imperfection amplitude can be controlled (manufacturing tolerances), **shape cannot!**



LSK ASYMPTOTICS – IMPERFECT CASE – EQUILIBRIUM

$$u = \overset{0}{u}(\lambda) + \xi \overset{1}{u} + v, \quad v \in \mathcal{N}^\perp, \quad \xi \in \mathbb{R}; \quad \xi \equiv (u - \overset{0}{u}, \overset{1}{u}), \quad \Delta\lambda \equiv \lambda - \lambda_c$$

$$\bar{\mathcal{E}}_{,v} \delta v = 0 \implies \bar{\mathcal{E}}_{,u} (\overset{0}{u}(\lambda_c + \Delta\lambda) + \xi \overset{1}{u} + v, \lambda_c + \Delta\lambda, \epsilon \bar{w}) \delta v = 0; \quad \text{equilibrium in } \mathcal{N}^\perp,$$

Expand about $(u, \lambda, w) = (u_c, \lambda_c, 0)$ to find $v(\xi, \Delta\lambda, \epsilon)$, where :

$$v(\xi, \Delta\lambda, \epsilon) = \xi v_\xi + \Delta\lambda v_\lambda + \epsilon v_\epsilon +$$

$$\frac{1}{2} [\xi^2 v_{\xi\xi} + 2\xi \Delta\lambda v_{\xi\lambda} + 2\xi \epsilon v_{\xi\epsilon} + (\Delta\lambda)^2 v_{\lambda\lambda} + 2\Delta\lambda \epsilon v_{\lambda\epsilon} + \epsilon^2 v_{\epsilon\epsilon}] + \dots$$

Expand about $(u, \lambda, w) = (u_c, \lambda_c, 0)$, using $v(\xi, \Delta\lambda, \epsilon)$, to find $\epsilon(\xi, \Delta\lambda)$ from :

$$\bar{\mathcal{E}}_{,\xi} = 0 \implies \bar{\mathcal{E}}_{,u} (\overset{0}{u}(\lambda_c + \Delta\lambda) + \xi \overset{1}{u} + v, \lambda_c + \Delta\lambda, \epsilon \bar{w}) \overset{1}{u} = 0; \quad \text{equilibrium in } \mathcal{N}.$$



LSK ASYMPTOTICS – IMPERFECT CASE – EQUILIBRIUM

$$O(\xi) : (\mathcal{E}_{,uu}^c v_\xi) \delta v = 0 \implies v_\xi = 0, \quad (\mathcal{E}_{,uu}^c \text{ unique eigenvalue : } \overset{1}{u})$$

$$O(\Delta\lambda) : (\mathcal{E}_{,uu}^c v_\lambda + \mathcal{E}_{,uu}^c (d\overset{0}{u}/d\lambda)_c + \mathcal{E}_{,u\lambda}^c) \delta v = (\mathcal{E}_{,uu}^c v_\lambda) \delta v = 0 \implies v_\lambda = 0, \quad (\text{same})$$

$$O(\xi^2) : (\mathcal{E}_{,uu}^c v_{\xi\xi} + (\mathcal{E}_{,uuu}^c \overset{1}{u}) \overset{1}{u}) \delta v = 0$$

$$O(\xi\Delta\lambda) : (\mathcal{E}_{,uu}^c v_{\xi\lambda} + (\mathcal{E}_{,uuu}^c (d\overset{0}{u}/d\lambda)_c + \mathcal{E}_{,uu\lambda}^c) \overset{1}{u}) \delta v = 0$$

$$O((\Delta\lambda)^2) : (\mathcal{E}_{,uu}^c v_{\lambda\lambda} + (\mathcal{E}_{,uuu}^c (d\overset{0}{u}/d\lambda)_c)(d\overset{0}{u}/d\lambda)_c + 2\mathcal{E}_{,uu\lambda}^c (d\overset{0}{u}/d\lambda)_c + \mathcal{E}_{,u\lambda\lambda}^c + \mathcal{E}_{,uu}^c (d^2\overset{0}{u}/d\lambda^2)_c) \delta v = (\mathcal{E}_{,uu}^c v_{\lambda\lambda}) \delta v = 0 \implies v_{\lambda\lambda} = 0, \quad (\text{same})$$

NOTE A : $O(\xi^n \Delta\lambda^m \epsilon^0)$ terms same as perfect case since at $\epsilon = 0$: $\bar{\mathcal{E}}(u, \lambda, w) = \mathcal{E}(u, \lambda)$

NOTE B : Highlighted terms λ derivatives of principal equilibrium : $\mathcal{E}_{,u}^c(\overset{0}{u}(\lambda), \lambda) \delta u = 0$



LSK ASYMPTOTICS – IMPERFECT CASE – EQUILIBRIUM

$$O(\epsilon) : (\mathcal{E}_{,uu}^c v_\epsilon + \bar{\mathcal{E}}_{,uw}^c \bar{w}) \delta v = 0$$

$$O(\xi\epsilon) : (\mathcal{E}_{,uu}^c v_{\xi\epsilon} + (\mathcal{E}_{,uuu}^c v_\epsilon + \bar{\mathcal{E}}_{,uuw}^c \bar{w})^1_u) \delta v = 0$$

$$O(\epsilon\Delta\lambda) : (\mathcal{E}_{,uu}^c v_{\lambda\epsilon} + (d\mathcal{E}_{,uu}/d\lambda)_c v_\epsilon + (d\bar{\mathcal{E}}_{,uw}/d\lambda)_c \bar{w}) \delta v = 0$$

$$O(\epsilon^2) : (\mathcal{E}_{,uu}^c v_{\epsilon\epsilon} + (\mathcal{E}_{,uuu}^c v_\epsilon) v_\epsilon + 2(\bar{\mathcal{E}}_{,uuw}^c \bar{w}) v_\epsilon + (\bar{\mathcal{E}}_{,uww}^c \bar{w}) \bar{w}) \delta v = 0$$

$$0 = \epsilon(\bar{\mathcal{E}}_{,uw}^c \bar{w})^1_u + \frac{1}{2}[\xi^2((\mathcal{E}_{,uuu}^c u)^1_u)^1_u + 2\xi\Delta\lambda((d\mathcal{E}_{,uu}/d\lambda)_c u)^1_u +$$

$$2\xi\epsilon((\mathcal{E}_{,uuu}^c v_\epsilon + \bar{\mathcal{E}}_{,uuw}^c \bar{w})^1_u)^1_u + 2\epsilon\Delta\lambda((d\mathcal{E}_{,uu}/d\lambda)_c v_\epsilon + (d\bar{\mathcal{E}}_{,uw}/d\lambda)_c \bar{w})^1_u +$$

$$\epsilon^2((\mathcal{E}_{,uuu}^c v_\epsilon) v_\epsilon + 2(\bar{\mathcal{E}}_{,uuw}^c \bar{w}) v_\epsilon + (\bar{\mathcal{E}}_{,uww}^c \bar{w}) \bar{w})^1_u] +$$

$$\frac{1}{6}[\xi^3(((\mathcal{E}_{,uuuu}^c u)^1_u)^1_u + 3\mathcal{E}_{,uu}^c v_{\xi\xi})^1_u + \dots] + \dots$$



LSK ASYMPTOTICS – IMPERFECT CASE – EQUILIBRIUM

Assuming $(\bar{\mathcal{E}}_{,uw}^c \bar{w})^1_u \neq 0$, use imperfection amplitude $\epsilon(\xi, \Delta\lambda)$ in equilibrium : $\bar{\mathcal{E}}_\xi = 0$

$$\epsilon(\xi, \Delta\lambda) = [((d\mathcal{E}_{,uu} / d\lambda)_c \bar{u})^1_u / (\bar{\mathcal{E}}_{,uw}^c \bar{w})^1_u] \begin{cases} (\lambda_1 \xi^2 - \xi \Delta\lambda) + \dots & \text{for } ((\mathcal{E}_{,uuu}^c \bar{u})^1_u)^1_u \neq 0 \\ (\frac{\lambda_2}{2} \xi^3 - \xi \Delta\lambda) + \dots & \text{for } ((\mathcal{E}_{,uuu}^c \bar{u})^1_u)^1_u = 0 \end{cases}$$

- To avoid fractional expansions, one must find the level sets of the imperfection amplitude, i.e. express ϵ in terms of ξ and $\Delta\lambda$.
- There is no sensitivity to an imperfection w unless it has a component along the critical mode of the corresponding perfect system
- NOTE: For typical system with random imperfection shape, it always has a component along the critical mode of the corresponding perfect system



LSK ASYMPTOTICS – IMPERFECT CASE – STABILITY

$$(\bar{\mathcal{E}}_{,uu} (\overset{0}{u}(\lambda_c + \Delta\lambda) + \xi \overset{1}{u} + v(\xi, \Delta\lambda, \epsilon(\xi, \Delta\lambda)), \lambda_c + \Delta\lambda, \epsilon(\xi, \Delta\lambda) \bar{w}) \bar{x}(\xi, \Delta\lambda)) \delta u = \\ = \bar{\beta}(\xi, \Delta\lambda) (\bar{x}(\xi, \Delta\lambda), \delta u), \text{ with } \bar{\beta} \text{ eigenvalue, } \bar{x} (\|\bar{x}\| = 1) \text{ eigenvector of : } \bar{\mathcal{E}}_{,uu}$$

$$\text{Where : } \bar{\beta}(\xi, \Delta\lambda) = \xi \bar{\beta}_\xi + \Delta\lambda \bar{\beta}_\lambda + \frac{1}{2} (\xi^2 \bar{\beta}_{\xi\xi} + 2\xi \Delta\lambda \bar{\beta}_{\xi\lambda} + (\Delta\lambda)^2 \bar{\beta}_{\lambda\lambda}) + \dots$$

$$\text{Where : } \bar{x}(\xi, \Delta\lambda) = \bar{x}_0 + \xi \bar{x}_\xi + \Delta\lambda \bar{x}_\lambda + \frac{1}{2} (\xi^2 \bar{x}_{\xi\xi} + 2\xi \Delta\lambda \bar{x}_{\xi\lambda} + (\Delta\lambda)^2 \bar{x}_{\lambda\lambda}) + \dots$$

$$O(1) : (\mathcal{E}_{,uu}^c \bar{x}_0) \delta u = 0, \quad (\bar{x}_0, \bar{x}_0) = 1 \implies \bar{x}_0 = \overset{1}{u}$$

$$O(\xi) : (\mathcal{E}_{,uu}^c \bar{x}_\xi + (\mathcal{E}_{,uuu}^c \overset{1}{u}) \overset{1}{u}) \delta u = \bar{\beta}_\xi (\overset{1}{u}, \delta u)$$

$$\text{using : } \delta u = \overset{1}{u} \implies \bar{\beta}_\xi = ((\mathcal{E}_{,uuu}^c \overset{1}{u}) \overset{1}{u}) \overset{1}{u}$$

$$\text{using : } \delta u = \delta v \implies (\mathcal{E}_{,uu}^c \bar{x}_\xi + (\mathcal{E}_{,uuu}^c \overset{1}{u}) \overset{1}{u}) \delta v = 0 \implies \bar{x}_\xi = v_{\xi\xi}$$



LSK ASYMPTOTICS – IMPERFECT CASE – STABILITY

$$O(\Delta\lambda) : (\mathcal{E}_{,uu}^c \bar{x}_\lambda + (d\mathcal{E}_{,uu}/d\lambda)_c \bar{u}^1) \delta u = \bar{\beta}_\lambda(\bar{u}^1, \delta u)$$

$$\text{using : } \delta u = \bar{u}^1 \implies \bar{\beta}_\lambda = ((d\mathcal{E}_{,uu}/d\lambda)_c \bar{u}^1) \bar{u}^1$$

$$\text{using : } \delta u = \delta v \implies (\mathcal{E}_{,uu}^c \bar{x}_\lambda + (d\mathcal{E}_{,uu}/d\lambda)_c \bar{u}^1) \delta u = 0 \implies \bar{x}_\lambda = v_{\xi\lambda}$$

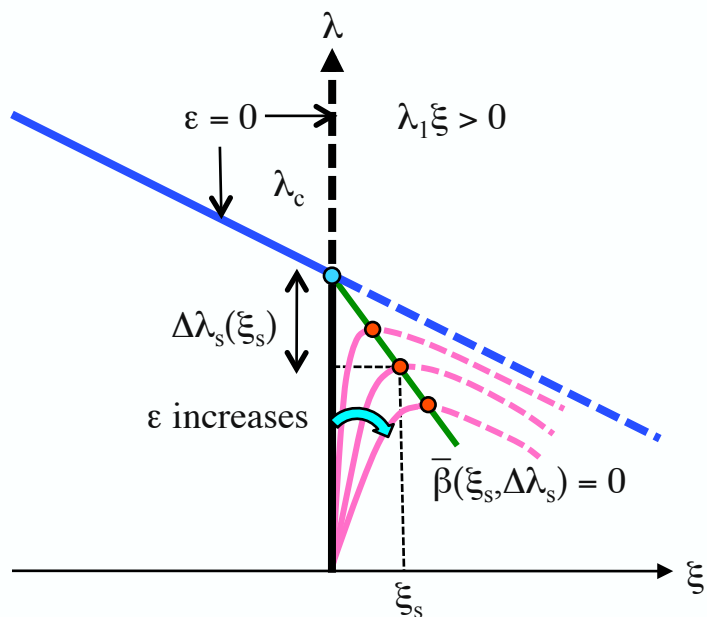
$$O(\xi^2) : \left(\frac{1}{2} (((\mathcal{E}_{,uuuu}^c \bar{u}^1) \bar{u}^1) \bar{u}^1 + \mathcal{E}_{,uuu}^c v_{\xi\xi}) \bar{u}^1 + (\mathcal{E}_{,uuu}^c v_{\xi\xi}) \bar{u}^1 + \frac{1}{2} \mathcal{E}_{,uu}^c \bar{x}_{\xi\xi} \right) \delta u = \frac{1}{2} \bar{\beta}_{\xi\xi}(\bar{u}^1, \delta u)$$

$$\text{using : } \delta u = \bar{u}^1 \implies \bar{\beta}_{\xi\xi} = (((\mathcal{E}_{,uuuu}^c \bar{u}^1) \bar{u}^1 + 3\mathcal{E}_{,uuu}^c v_{\xi\xi}) \bar{u}^1) \bar{u}^1$$

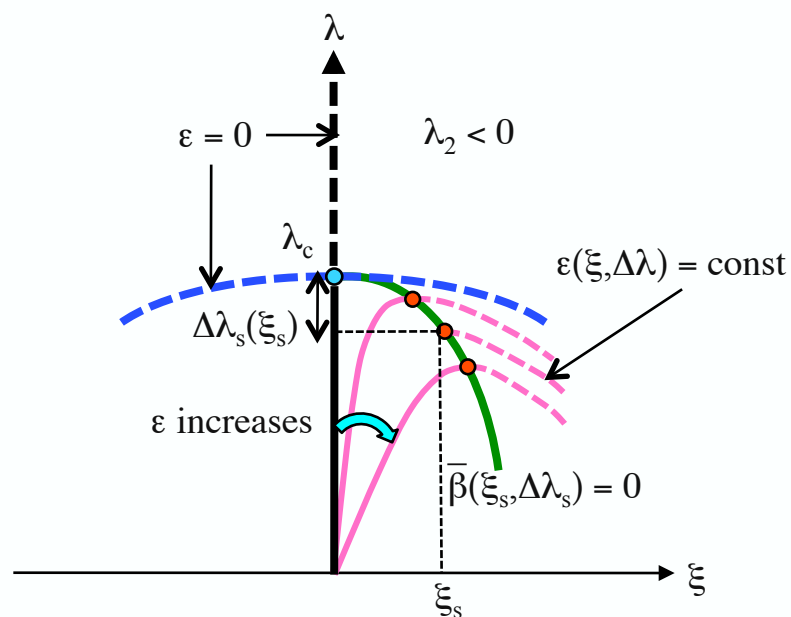
$$\bar{\beta}(\xi, \Delta\lambda) = [((d\mathcal{E}_{,uu}/d\lambda)_c \bar{u}^1) \bar{u}^1] \begin{cases} (-2\lambda_1 \xi + \Delta\lambda) + \dots & \text{for } ((\mathcal{E}_{,uuu}^c \bar{u}^1) \bar{u}^1) \bar{u}^1 \neq 0 \\ (-\frac{3}{2} \lambda_2 \xi^2 + \Delta\lambda) + \dots & \text{for } ((\mathcal{E}_{,uuu}^c \bar{u}^1) \bar{u}^1) \bar{u}^1 = 0 \end{cases}$$



LSK ASYMPTOTICS – IMPERFECT CASE – RESULTS



Asymmetric bifurcation – Imperfect Case



Symmetric bifurcation – Imperfect Case



LSK ASYMPTOTICS – IMPERFECT CASE – LOAD DROP

$$\bar{\beta}(\xi, \Delta\lambda_s(\xi)) = 0, \quad \Delta\lambda_s(\xi) = s_1\xi + \frac{s_2}{2!}\xi^2 + \frac{s_3}{3!}\xi^3 + O(\xi^4), \quad \text{locus of limit points}$$

$$\Delta\lambda_s(\xi) = \begin{cases} 2\lambda_1\xi + O(\xi^2) & \text{for } ((\mathcal{E},_{uuu}^c \bar{w})^1_u)^1_u \neq 0 \\ \frac{3}{2}\lambda_2\xi^2 + O(\xi^3) & \text{for } ((\mathcal{E},_{uuu}^c \bar{w})^1_u)^1_u = 0 \end{cases}$$

Using the expansion for the imperfection amplitude $\epsilon(\xi, \Delta\lambda_s)$; Assume : $\epsilon > 0$

$$\Delta\lambda_s(\epsilon) = \begin{cases} -2(|\lambda_1|)^{1/2} \left[\frac{\epsilon |(\bar{\mathcal{E}},_{uw}^c \bar{w})^1_u|}{((-d\mathcal{E},_{uu} / d\lambda)_{c\bar{u}}^1_u)^1_u} \right]^{1/2} + O(\epsilon) & \text{for } ((\mathcal{E},_{uuu}^c \bar{w})^1_u)^1_u \neq 0, \\ \frac{3}{2}(\lambda_2)^{1/3} \left[\frac{\epsilon(\bar{\mathcal{E}},_{uw}^c \bar{w})^1_u}{((-d\mathcal{E},_{uu} / d\lambda)_{c\bar{u}}^1_u)^1_u} \right]^{2/3} + O(\epsilon) & \text{for } ((\mathcal{E},_{uuu}^c \bar{w})^1_u)^1_u = 0. \end{cases}$$

IMPORTANT : $\Delta\lambda_s(\epsilon) < 0$ if $\lambda_1(\bar{\mathcal{E}},_{uw}^c \bar{w})^1_u < 0$ (assym. bif.) or $\lambda_2 < 0$ (sym. bif).



LSK ASYMPTOTICS – IMPERFECT CASE – REVIEW

- Behavior of **imperfect** structure near critical load can be **analyzed** by **asymptotic expansion** of equilibrium solution.
- **Bifurcation** point in perfect case is **replaced** by **limit points** in imperfect case.
- Method determines the limit points (where stability changes) of imperfect structure and the **load drop** $\Delta\lambda_s$ from the critical load of the perfect structure λ_c to the maximum load of the imperfect one λ_s .
- Recall that in real structures the amplitude ε can be controlled but **not** the shape w .
- Load drop is **maximized** when **imperfection has the shape of the eigenmode**.
- Structures are **imperfection sensitive (i.e. $\Delta\lambda_s < 0$)** for **asymmetric** or **symmetric subcritical** bifurcations (load max exists for the equilibrium path through zero load); $\Delta\lambda_s = O(\varepsilon^{1/2})$ for asymmetric case and $\Delta\lambda_s = O(\varepsilon^{2/3})$ for subcritical symmetric case.
- **NOTE:** Imperfection can occur in **any property** (material or geometric) that **destroys** the **symmetry** of the system; all related asymptotic analyses are equivalent.